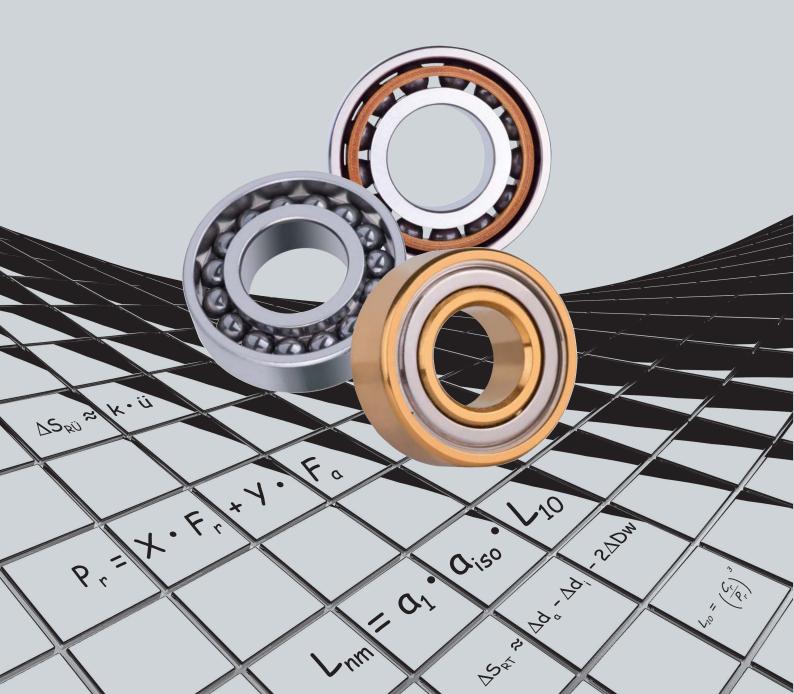




High-Precision Ball Bearings Product Catalogue





Designation system of radial ball bearings – metric / inch



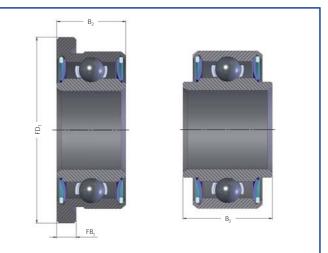


	-		-	LE	625	5		-	P		C
	HY		SS	F	3/1	6		-Z	ABEC		К
	ZO		SV	E	625/60	3938		-2Z			
			S		-			-RZ			
			SA					-RS			
			Ν					-VZ			
			NZ					-VS			
								-TS			
-	Steel balls	-	100Cr6	LE Bearing unit	625	Metric	-	Open ball bearings	Standard tolerance grade	Metric o bearing	deep groove radial
ШΥ	Ceramic	SS	X65Cr13	F Flange	3/16	Inch	-Z	Single shield	PO or ABEC1	-	Standard clearance
	balls made from	sv	X30CrMoN15-1	E Extended inner ring	625/XXXXXX	Acc. to drawing	-2Z	Double shield	not marked	C2 C3	Narrower than standard Slightly increased radial
	Si ₃ N ₄	S	440C	inner nng		urawing	-RZ	Single Perbunan rubber shield,	P tolerance grade for metric	C4	clearance Increased radial clearance
zo	Ceramic balls	SA	Antimagnetic material					non-contact	bearings in P6 , P5 , P4 and P2	C5	Strongly increased radial clearance
	made from ZrO ₂		mbination balls				-RS	Single Perbunan rubber contact seal	ABEC		ct values depend on the
		Ν	Full ceramic bearings				-vz	Single Viton shield,	tolerance grade for inch bearings		dimensions, see capter ssification of radial
			(balls, IR, AR) of silicon nitride					non-contact	in ABEC3, ABEC5 etc.	clearand	
		NZ	Full ceramic				-VS	Single Viton contact seal	Special tolerance	C1/5	radial clearance: f.e. 1 to 5 µm
			bearings (balls, IR, AR)				-TS	Single Teflon®	grades: ABEC9P,	C4/8	4 to 8 µm 5 10 to 15 µm
			made from zirconium oxide				10	contact seal	P4A, P4S,		14 to 20 µm
											ep groove radial bearings
										Defined	radial clearance: f.e. 0 to .0002"
										K02	.0001" to .0003"
										K46 K58	.0004" to .0006" .0005" to .0008"
										D	Followed a by number
											indicates contract angle
											ball bearings
										C E	Contact angle 15° Contact angle 25°
			her materials								
		ava	ilable on request								

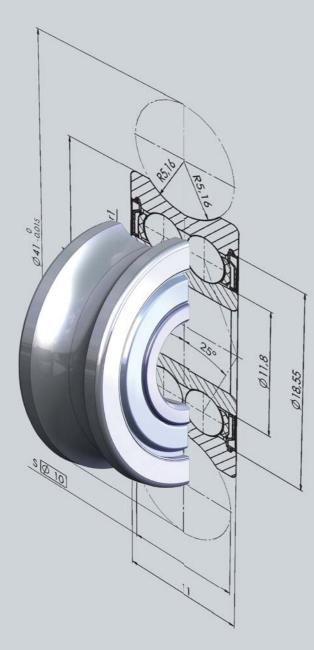


GPR GPA R()	X XB XD X4 X4B X4D	-1 -2 -3 -4	/ L M S	Е Ј Ј1 ТХНВ Т19НВ АС1ТА	– % MG	G L L299 B
 GPR Noise test (standard 100%) GPA Axial vibration test R() Followed by a number indicates starting torque with standard load, max. 16 μNm 	 X Bore and outside diameter graded in 2 classes XB Bore graded in 2 classes XD Outside diameter graded in 2 classes XA Bore and outside diameter graded in 4 classes X4B Bore graded in 4 classes X4D Outside diameter graded in 4 classes X4D Outside diameter graded in 4 classes 	 Back to back (O-arrangement) Face to face (X-arrangement) Tandem Universally paired Example Spindle ball bearings: UM (= universally mate medium preload) 	dial bearings: ngement with load)	Deep groove radial bearings E 2-pc. steel retainer J 2-pc. stainl. steel retainer J1 J1 2-pc. stainl. steel retainer Teflon®.laminated TXHB Machined one-piece snap retainer, X stands for a number and defines the material T19HB Machined synthetic snap retainer made from PAI-PTFE-cg Other retainer variants see chapter "Retainers for miniature ball bearings" Full complement ball bearing VAC1 Outer ring shoulder ground Spindle ball bearings AC1 Outer ring shoulder ground AC2 Inner ring shoulder ground AC2 Inner ring shoulder ground AC2 Inner ring shoulder ground AC2 Only in connection with solid retainer or full-complement Example: AC1TA Machined solid retainer made from fabric- reinforced phenolic resin	Standard quantity % Lubricant quantity in % of the free space only for lubricated bearings)	L Oil









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Spindle ball bearings

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Our company

As a global corporation with more than 500 employees, GRW is headquartered in Rimpar near Würzburg with assembly facilities in Prachatice (Czech Republic) and two offices in the USA.

GRW is the premier developer and manufacturer of miniature precision ball bearings, assemblies and accessory parts utilizing state of the art equipment and manufacturing processes. We specialise in the production of high precision, small, miniature and instrument bearings as well as spindle bearings and bearing units. GRW also welcomes the opportunity to design, develop and produce customised applications using customer specifications.

Our radial ball bearings range in bores from 1 mm to 35 mm with outer diameters from 3 mm to 47 mm meeting any need from low to high volume standard applications.

GRW bearings are produced in both metric and inch dimensions making them truly applicable to any customer in the world. Whether your application requires high or low quantities or customised specifications, you can always rely upon GRW to meet any requirement or challenge.

GRW complies with the highly recognised standard ISO certification, DIN EN ISO 9001:2008 for quality in process and performance.

Preface

"Miniature precision meets extreme demands"

GRW high-precision ball bearings are used in measurement and control technologies, medical & dental technologies, vacuum applications, electric motors, and high-tech aerospace industries.

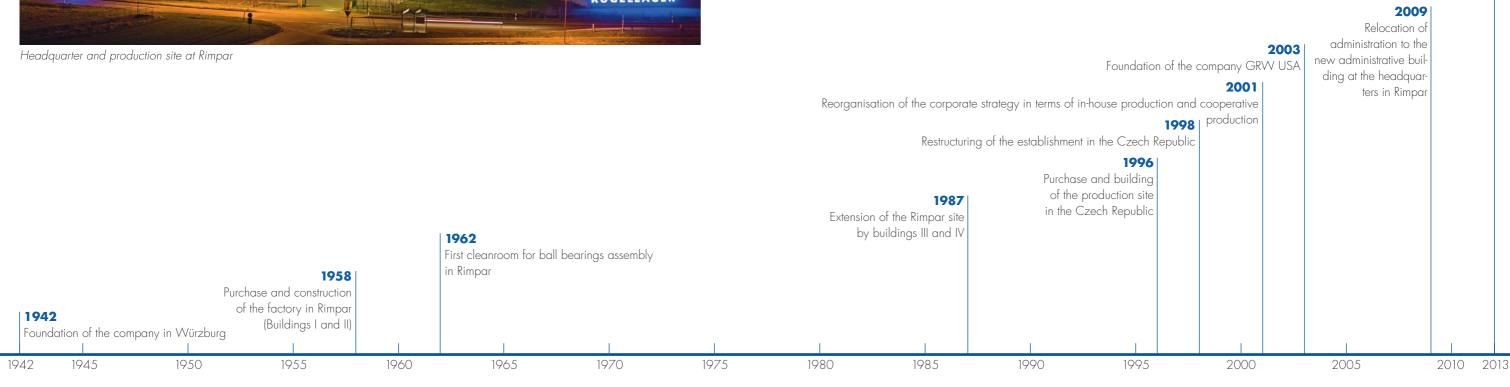
This GRW Product Catalog provides extensive detail on our products for standard industry solutions and customised systems to meet our customers' most demanding challenges.

Our new program, EXTREME, is designed for applications that go far beyond the standard product solution. In fact, GRW products are optimised to our EXTREME standards. Which means we not only meet but also surpass your specifications for longer life, higher speed and load ratings and do so with incredibly dependable customer service.

See page 79 to 83 of this product catalogue for details on this new program.



www.grw.de



Contact: +49 (0) 9365/819 - 440



We can do even better - just challenge us. Our sales engineers will be happy to advise you. We are looking forward to your call: +49 (0) 93 65/819 - 440



2013

Construction of the new production site in the Czech Republic and opening of a new sales office on the East Coast of the USA

| 3



Materials for rings and balls

Our ball bearings are manufactured by using technological advancements in steel production and heat treatment. Our ball bearings are made of chrome steel (100Cr6), stainless steel (X65Cr13), or high corrosion-resistant steel (X30Cr/MoN 15-1). It is now possible to achieve comparable load ratings for all these steel types.

Ceramic balls, e.g. hybrid ball bearings, can be used in all versions as required by your application.



Materials for rings and balls

Hybrid ball bearings

GRW hybrid, or ceramic, ball bearings are made of one of the steels mentioned above as well as silicon nitride (Si_3N_4) or zirconium oxide (ZrO_2), that offers specific benefits.

They are used most commonly in dental handpieces, spindle bearings and vacuum pumps to extend speed limits or increase bearing stiffness.

Using GRW \rm{Si}_3N_4 ceramic balls reduces static load rating by 30%, while dynamic load rating remains unaffected.

The low affinity to other materials allows a particularly low adhesive wear. As a result, hybrid or ceramic bearings show an extended lifetime when used in mixed-friction applications.

Prefix	Unit	-	SS	sv	НҮ	ZO
DIN		100Cr6	X65Cr13	X30CrMoN 15-1	Si ₃ N ₄	ZrO ₂
DIN		1.3505	1.4037	1.4108		
SAE		52100				
Properties						
Density	[g/cm ³]	7.81	7.7	7.7	3.2	6.0
Hardness	[HRC]	> 60	> 58	> 58	> 75	> 69
E module	[GPa]	212	220	223	320	200
Expansion coefficient	[x 10 ⁻⁶ °C]	11.0	10.5	10.4	3.0	10.5
Corrosion resistance	[-]	limited	good	very good	very good	good
Electrical conductivity	[-]	Conductor	Conductor	Conductor Conductor Insulat		Insulator
Magnetism	[-]	magnetic	magnetic	magnetic	non magnetic ⁽¹⁾	non magnetic

⁽¹⁾ May contain magnetic parts for production technology reasons

Our sales engineers will gladly inform you about the chemical resistance of the materials. Subject to change due to technical improvement.

Closures

Integrated ball bearing shields and seals provide two vital purposes: to prevent dirt and foreign particles from infiltration and to prevent lubricants from leaking out.

Non-contact shields

Together with the shoulder of the inner ring, the closure creates a narrow gap. Similar to open ball bearings, this closure neither increases running friction nor limits the maximum permissible speed because the shields do not touch the inner ring. This is sufficient for most applications. Shields prevent contamination with dirt particles but cannot achieve a hermetic seal.

Metal shields Z

For the majority of our bearings, shields are stamped from corrosion-resistant steel. They are fastened to the outer ring by means of a circlip and can thus be removed. Bearings can also be fitted with pressed-in shields made from a deep drawn steel sheet; these shields cannot be removed.

RZ/VZ non contact rubber shield

The RZ closure is made of synthetic buna N rubber with a steel support shield and can be used at temperatures from -30 °C to +120 °C.

The VZ closure is made of synthetic Viton fluoroelastomer with steel support shield and can be used at temperatures from -20 °C to +230 °C.

Both shield types are secured by snap fit.

Contact seals

This type of seal touches the shoulder of the inner ring, causing an increase in start up and running torque. Teflon[®] seals can be used at working temperatures of -240 °C to +300 °C. The friction is lower than for rubber seals due to the low friction combination (PTFE/ steel) and the low contact force of the sealing lip.

Teflon[®] seal TS

The TS seal is made of a glass-fiber reinforced Teflon[®] sheet that is fastened in the outer ring by means of a circlip.



TS seals are universally resistant to chemicals. Bearings using TS seals are normally made of corrosion-resistant steel. In appropriately large quantities, TS seals can also be made available for chrome steel bearings.

RS/VS seals

The RS seal is made of synthetic buna N rubber with a steel support shield and can be used at temperatures from -30 °C to +120 °C.

The VS seal is made of synthetic Viton fluoroelastomer with a steel support shield and can be used at temperatures from -20 °C to +230 °C.

Both seal types are secured by snap fit.

Custom Shields and Seals

GRW can also manufacture custom accessories and combinations of different shields and seals to meet your specifications.

For improved sealing effect between steel shields and outer ring GRW offers a special laminated shield.

In this context we would like to point out that certain lubricants cannot be used with all closures. Please consult our sales engineers about difficult applications.





Retainers for miniature ball bearings

Retainers are vital for efficient operation of ball bearings. They keep the balls separated and evenly spaced, ensuring a uniform distribution of load there by reducing heat thus enhancing the life expectancy of the bearing.

The retainer guides the balls in the load-free zone and prevents the balls from dropping out of separable bearings. Using our customised designs and

materials, retainers can be manufactured to meet any application. We recommend usage of two-part ribbon retainer for the majority of applications.

In this context we would like to point out that certain lubricants cannot be used with all retainers.

See the following list for our range of different retainers:

GRW retainer designation	Illustration	Description/ material	Scope of application / purpose
E J J1		Two-piece retainer made from – steel sheet (E) – stainless steel sheet (J) – stainless steel sheet, Teflon [®] -laminated (J1)	Standard retainer for deep groove radial bearings. For stainless ball bearings: retainer always made from stainless steel sheet.
		Retainer closing types: – without additional sign = standard – F = retainer tightly closed – L = retainer loosely closed	To avoid torque peaks as far as possible, this retainer can also be mounted in a loosely closed condition.
Η		One-piece snap-type retainer made of stainless steel	For deep groove radial bearings. Used primarily for small ball bearings and low to medium speeds.
TNH		One-piece molded synthetic snap retainer	For deep groove radial bearings in medium speed range with good running and torque characteristics. Working temperature from -30°C to +80 °C, short term up to +100 °C.
ТN9Н	0	One-piece molded synthetic snap retainer made from glass fiber reinforced plastic	For deep groove radial bearings in a speed range above that of the TNH retainer. Working temperature from -30°C to +120 °C, short term up to +180 °C.
THA THB	<u>A</u>	Machined one-piece snap retainer made from fiber-reinforced phenolic resin. A = outer ring guided B = guided on inner ring	For deep groove radial bearings with very high speeds. High rigidity and emergency running properties. Working temperature from −50°C to +130°C. Can be impregnated with oil.
ТХНА ТХНВ		Machined one-piece snap retainer made from a special material. X stands for a number and defines the material. A = outer ring guided B = guided on inner ring	For deep groove radial bearing with very high speeds. High rigidity and emergency running properties. Working temperature, depending on the material, up to +250°C or even +300°C.

GRW retainer designation	Illustration	Description/ material	Scope of application / purpose
L1T L2T	E B	L1T = outer ring separable, guided on inner ring L2T =inner ring separable, outer ring guided	For separable angular contact ball bearings/spindle ball bearings with highest speeds. High rigidity. Working temperature from –50 °C to +130 °C. Can be impregnated with oil.
L1TX L2TX	E B	L1TX = outer ring separable, guided on inner ring L2TX = inner ring separable, outer ring guided X stands for a number and defines the material.	For separable angular contact ball bearings/spindle ball bearings with highest speeds. High rigidity and emergency running properties. Working temperature, depending on the material, up to +250 °C or even +300 °C.
TA/TB	\bigcirc	Machined one-piece solid retainer made from fiber-reinforced phenolic resin. A = outer ring guided B = guided on inner ring Only together with AC types. Cannot be disassembled.	For angular contact ball bearings/ spindle ball bearings with highest speeds. High rigidity and emergency running properties. Working temperature from –50 °C to +130 °C. Can be impregnated with oil.
TXA/TXB AC2TXA/TXB	\bigcirc	Machined one-piece solid retainer made from a special material. X stands for a number and defines the material. A = outer ring guided B = guided on inner ring Only together with AC types. Cannot be disassembled.	For angular contact ball bearings/ spindle ball bearings with highest speeds. High rigidity and emergency running properties. Working temperature, depending on the material, up to +250 °C or even +300 °C.
VAC1 VAC2		Full complement ball bearing, without retainer, cannot be disassembled. VAC 1 = one shoulder relieved on outer ring VAC2 = one shoulder relieved on inner ring Outer ring or inner ring shoulder ground on one side.	Used for medium speeds, high radial loads and high axial loads in one direction.
VF		Full complement ball bearing, without retainer, cannot be disassembled, with filling slot for inserting the balls.	Used for medium speeds and high radial loads.

As not every retainer is available for all sizes of ball bearings, please contact us for additional information. On request, we will also gladly recommend other ball bearing and retainer designs as well as retainer materials for special requirements.

GRW offers some of the highest performance synthetic materials including Vespel[®], Torlon[®], PEEK, PTFE and **Meldin**[®] as well as various metallic materials and phenolic resins.

In addition to using proven materials, GRW, in close cooperation with its customers and suppliers, is



constantly developing new options or enhancing existing variations. As a result, GRW is the sole owner of some exclusive licenses and patents for using specifically developed retainer materials such as PAI-PTFE-cg.



Lubricants

Why do bearings need lubricants?

Miniature ball bearings are perfect for high stress environments, but require special lubricants to minimise wear in order to increase operational life, performance, and safety of the product.

GRW lubricants provide permanent lubrication to minimise sliding friction between balls, rings and retainer. This prevents excessive wear and thermal overheating, protecting balls and raceway from micro-welding and thereby extending operational life while reducing running noise. The application determines the best type of lubrication to use.

Grease Lubrication

Thanks to its ability to dispense a lubricating film over time, grease lubricants offer an additional advantage when being used in maintenance-free applications.

Most of GRW bearings are grease-lubricated, with approximately 300 different greases to select from. The standard recommended amount of grease (lubricant quantity) is one-third (33%) of the remaining free space in the bearing. Grease quantities deviating from this standard are indicated in the bearing part number just before the type of lubricant, preferably in percent or alternatively in milligrams.



Furthermore, our customers can choose other special treatments for grease applications, for example a dispersion or a thin defined layer of grease. Here the designation system differentiates between DF (thin film), MF (medium film) and SF (strong film).

Oil lubrication

Oil is primarily used in applications where a minimal torque is required. In particular, high speed spindle bearings are typically lubricated with high performance oils.

When compared to grease lubrication, oil lubrication sometimes uses a dispersion of oil and a solvent achieving a better distribution of oil throughout the bearing.

With more than 100 special oils to choose from, GRW can help you to select the oil that perfectly matches your application. If no special lubrication is needed, all of our bearings whether open or shielded, are preserved with light instrument oil when they leave our factory.

Proper Lubrication Practices

At GRW all bearings are lubricated during final assembly under clean-room conditions. Since dust particles can cling to the oiled or greased bearings, it is important that the customer maintains a high standard of cleanliness in his application. In addition we recommend using a clean-room for removal of the bearings from their package and during assembly.

With greased bearings, the specified quantity of lubricant, accurate to milligrams, is injected directly into specified locations of the miniature ball bearing. Usually the lubricant is injected from only one side: however it is also possible to lubricate each bearing from both sides for better distribution.

For lubrication with standard oils, the oil is poured over the bearing which is then spun. Alternatively, a specified oil quantity can be directly injected into the bearing.

Solid Lubricants

Non-lubricated bearings may be used in certain applications and are also available from GRW. These non-lubricated bearings are typically required for ultra-high vacuum (UHV) temperature extremes and for applications in aviation and aerospace. Here the operating conditions go beyond the functional limits of oil and grease lubricants. The use of a bearing without a protective lubricant will negatively impact its tribological system; however lubrication with solids is a viable alternative.

GRW offers its customers a variety of different dry film coatings. Applying thin layers of precious metals, graphite or Wolfratherm[®] (MoS₂) provides protection and lubrication for the bearing.

For oil or grease lubricated bearings, this process ensures reliable performance in case of lubricant deprivation (emergency running conditions). In GRW's part numbering system the surface treatment of bearing components is indicated by a "B", followed by a four-digit number code indicating the type of surface treatment.

Custom treatments

In addition to varying lubricants and surface treatments GRW can custom treat bearing components to improve tribological behaviour. For example, the phenolic retainer can be vacuum-impregnated with oil (up to 5% by weight).

The benefit of a vacuum-impregnated retainer is its ability to release small amounts of lubricant continually during operation. This process improves the general lubrication performance and ensures emergency running properties in lube deprived situations.



Lubricants in medical applications

Sterilisation (autoclaving) is mandatory for the correct use and maintenance of medical instruments according to the guidelines of the Robert-Koch Institute. This applies to the hygienic treatment of surgical devices and dental turbines that depend on miniature ball bearings.

GRW's stainless steel and retainer materials can easily withstand sterilisation in an autoclave subjected to superheated steam, where most lubricants do not survive. Combined with the extreme high speed stresses of dental turbines, these lubricants are required to provide exceptional surface adhesion and sterilisation resistance.

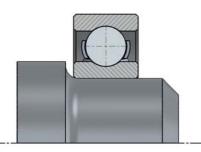
GRW bearings utilize a range of lubricants that are resistant to the sterilisation process. This makes them well suitable for dental and surgical devices and results in longer life under these extreme environmental conditions.



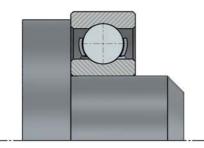
Shaft and housing shoulders

Certain design and assembly factors are critical for optimum performance of bearings. For instance, shaft and housing shoulders should accurately allow axial load to be transferred to the inner and outer ring without permitting the rings to tilt in opposite directions.

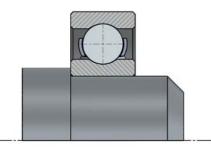
The associated dimension tables provide limits for the largest $(d_{a max})$ and the smallest $(d_{a min})$ permissible shoulder diameter for the inner ring and the largest permissible shoulder diameter for the outer ring $(D_{a max})$.



Wrong, Shaft radius bigger r_{s min}



Wrong, Shaft collar bigger $d_{a max}$

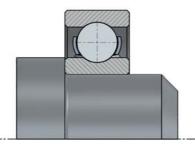


Wrong, Shaft collar smaller $d_{a \min}$

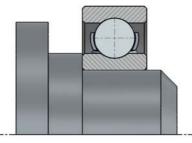
Note: Similar examples apply to bearing housings.

Please note the following considerations:

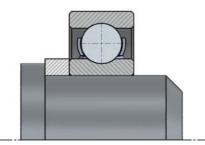
- The housing shoulder diameter for the outer ring must always be smaller than (D_{a max}) and the shaft shoulder diameter at the inner ring must not be smaller than (d_{a min}).
- The corner radius between fit and shoulder must not be larger than the corner clearance (r_{s min}) of the bearing. Here an undercut is preferable to a corner radius. The edge radii of the bearing are not designed as a locating surface for the bearing in any way.
- The axial runout of the mating surfaces should not be bigger than the maximum axial runout of the bearing used. Otherwise the function of the bearing will be compromised.



Right, Shaft radius smaller than $r_{s min}$



Right, Shaft collar with shoulder



Right, Support ring in place

Special installation configurations

Flanged bearings

Using miniature and instrument bearings with a flange on the outer ring offers several advantages.

Stepped housing bores, which make it impossible or very difficult to maintain accurate alignment of both bearing fits, are no longer necessary. There is also no need for the use of circlips, which create manufacturing difficulties in small housing bores or thin-walled housings.

Flanged bearings assembled in narrow housings, such as gearboxes, are particularly effective and with paired bearings the use of a flanged bearing simplifies the correct assembly and alignment of the bearing.

This allows the accurate axial positioning of the Duplex bearing pair.

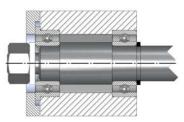
Bearings with extended inner rings

Bearings with an extended inner ring simplify design and mounting of various assemblies. Shims, washers and other spacers are not necessary. Stepped shafts are also redundant.

Bearings with reinforced outer ring

Ball bearings whose outer rings are supported by a correct housing fit can face the highest loads. To increase the load capacity of a bearing which is not pressed into a housing, it takes advantage of a reinforced outer ring. These types of bearings can be used as "rollers".





Proper installation, general



Assembly in narrow housings



Application of a Duplex bearing



Bearings with extended inner ring



Bearings with reinforced outer ring



Fitting tolerances

The fit of the bearing on the shaft and in the housing significantly affects the operational behavior of miniature ball bearings. When selecting fitting tolerances the following criteria should be considered:

Rotation conditions

Rings with circumferential load should have a tighter fit than rings with point load.

Circumferential load occurs when the ring is rotating and the load is static, or when the ring is static and the load is rotating.

Point load occurs when ring and load are both static, or when ring and load are both rotating in the same direction with equal speed. Please refer to the table "Shaft and housing fits by load type".

Running accuracy

The same high standards of accuracy and surface quality applicable to the bearings must be applied to the shaft and housing bore; refer to the overview "Accuracy of parts".

Loading

Higher loads require a tighter fit between the ball bearing, shaft and housing.

Temperature

There may be temperature differences between the bearing and mating components while the bearing is in operation, therefore dimensional changes caused by differential thermal expansion should be considered when selecting a bearing.

With miniature bearings it is very important to select the proper fit for the highest accuracy and reliability, hence only a close sliding or transition fit is generally required. All irregularities on the shaft or in the housing bore are directly transferred to the relatively thin(-walled) bearing rings.

To improve the fit it is possible to classify and sort the bore and outside diameters into groups (also refer to the chapter "Grading of bore and outside diameters"). The values shown in these tables "Shaft tolerances" and "Housing tolerances" are only valid for materials with the same expansion coefficient ($11 \times 10^{-6} \text{ 1/K}$). For different expansion coefficients, or when there are temperature differences between the bearing rings and the shaft or housing, a tolerance should be selected which ensures the appropriate fit at operating temperature.

Note: For certain environmental conditions an adhesive may be used to secure the bearing rings. Please contact our sales engineers for additional information.

Recommended fittings

The recommended fits listed below assume mean tolerances obtained from performance test data.

Shaft tolerances

Ball bearing bore Quality →	PO	Р5	Gra	Type of fit	
Tolerance in µm Tolerance in .0001 inch →	0/-8 0/-3	0/-5 0/-2	0/-2.5 0/-1	-2.5/-5 -1/-2	
Operating conditions					
Low load Medium speeds No oscillations	-5/-13 -2/-5	-5/-11 -2/-4	-5/-8 -2/-3	-8/-11 -3/-4	Slide fit
Low to medium loads Medium speeds Low oscillations	0/-8 0/-3	0/-6 0/-2.5	0/-3 0/-1.2	-3/-6 -1.2/-2.5	Tight fit
High loads High speeds Oscillations at high frequency	+4/-4 +1.6/-1.6	+4/-2 +1.6/-1	+4/+1 +1.6/+.4	+1/-2 +.4/-1	Press fit

Subject to change due to technical improvement.

Housing tolerances

Ball bearing bore Quality →	PO	P5	Grad	Type of fit	
Tolerance in µm Tolerance in .0001 inch →	0/-8 0/-3	0/-5 0/-2	0/-2.5 0/-1	-2.5/-5 -1/-2	
Operating conditions					
Low load Medium speeds No oscillations	+5/-3 +2/-1.2	+5/-1 +2/4	+5/+2 +2/+1	+2/-1 +1/4	Slide fit
Low to medium loads Medium speeds Low oscillations	0/-8 0/-3	0/-6 0/-2.5	0/-3 0/-1.2	-3/-6 -1.2/-2.5	Tight fit
High loads High speeds Oscillations at high frequency	-4/-12 -1.6/-5	-3/-9 -1.2/-3.5	-3/-6 -1.2/-2.5	-6/-9 -2.5/-3.5	Press fit

Subject to change due to technical improvement.

Note:

The information on this page applies to steel shafts and housings. If applicable, linear expansion coefficients of other materials (e.g. aluminium housings) must be taken into consideration for



other operating temperatures.

For more information on grading, refer to the chapter "Grading of bore and outside diameters".



Load ratings and L-10 life

The static radial load rating Cor

The basic static radial load rating (C_{0r}) applies to bearings which rotate at very slow speeds, which are subjected to slow oscillations or are stationary under load. Per DIN ISO 76, the basic static radial load rating is the static radial load corresponding to a calculated contact stress of 4200 N/mm² at the center of the contact ellipse of the most heavily loaded ball or raceway.

If the contact pressure exceeds this maximum permissible value, plastic deformation will occur affecting an efficient operation and the life of the bearing. The basic static radial load rating is the maximum allowable radial load for the bearing.

The basic static radial load rating for hybrid bearings with Si_3N_4 balls will be approximately 30% lower than for steel ball bearings.

Static bearing capacity

Static loads including radial and axial components must be converted into the static equivalent radial load (P_r). The static bearing load capacity (P_r) is the static radial load which causes the same contact stress at the center of the contact ellipse of the most heavily loaded ball or raceway which occurs under actual load conditions. It is defined as follows:



- P_r : Static equivalent radial load [N]
- X : 0.6
- Y : 0.5
- $\rm F_{\rm r}~$: Biggest radial load occurring [N]
- F_{a} : Biggest axial load occurring [N]
- Where: $P_r = F_r$ if $P_r < F_r$

Basic dynamic radial load rating C_r

According to DIN ISO 281, the basic dynamic load rating (C_r) for radial ball bearings is the constant radial load at which a sufficiently large group of apparently identical bearings can endure one million revolutions before showing evidence of material fatigue.

Fatigue load limit C_u

The fatigue load limit (C_u) is defined as the radial load below which no material fatigue will occur. For ball bearings manufactured with commonly used high-quality materials, the fatigue load limit is reached at a contact stress of approx. 1500 N/mm².

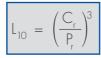
The load ratings calculated in this Product Catalogue have been computed using a curvature of 52–53 % according to DIN ISO 281. Depending on the bearing geometries, the actual load ratings may differ.

Nominal life L₁₀

The "nominal life" (L_{10}) of a group of apparently identical ball bearings is the life in millions of revolutions, or number of hours, that 90 percent of the group will complete or exceed before the first evidence of material fatigue occurs. For a single bearing, (L_{10}) also refers to the life associated with 90 percent reliability.

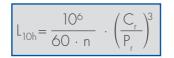
This calculation per ISO DIN 281 assumes identical operating conditions including a constant lubrication film separating the ball complement from the raceway during the entire life of the bearing.

The L-10 life of miniature ball bearings is calculated as follows:



- L₁₀ : basic rating life for a reliability of 90 % [10⁶ revolutions]
- C_r : basic dynamic radial load rating [N]
- ${\sf P}_{\!r}\,$: dynamic equivalent radial load fatigue occurs.

Taking a constant speed for granted, the number of revolutions can also be expressed as L-10 life in hours (L_{10h}) :



with

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- L_{10h}: basic rating life [h] n : speed of the inner ring [min⁻¹]
- C, : basic dynamic radial load rating [N]
- P_: dynamic equivalent radial load [N]
- $r_{\rm r}$: dynamic equivalent radial load [IN]

Extended modified rating life L_{nm}

In addition to the nominal life rating (L_{10}), DIN ISO 281 introduced an extended modified life rating (L_{nm}) and adds a life coefficient (a_1) as well as operating conditions (a_{ISO}). In application, life rating may be considerably higher or lower than the nominal L-10 life (L_{10}). The following correlation applies:

$a_{nm} = a_1 \cdot a_{ISO} \cdot L_{10}$

- L_{nm} : extended modified rating life [10⁶ revolutions]
- a₁ : Rating life coefficient for a requisite reliability deviating from 90 %
- $\label{eq:a_iso} \begin{array}{ll} \mbox{:} & \mbox{Rating life coefficient for consideration of operating conditions} \end{array}$
- L₁₀: basic rating life for a reliability of 90 % [10⁶ revolutions]

Rating life coefficient for Reliability a1 acc. DIN ISO 281

Reliability %	L _{nm}	a
90	L _{1Om}]
95	L _{5m}	0.64
96	L _{4m}	0.55
98	L _{3m}	0.47
98	L _{2m}	0.37
99	L _{lm}	0.25
99.2	L _{O.8m}	0.22
99.4	L _{O.6m}	0.19
99.6	L _{O.4m}	0.16
99.8	L _{O.2m}	0.12
99.9	L _{O.1m}	0.093
99.92	L _{0.08m}	0.087
99.94	L _{O.Oóm}	0.080
99.95	L _{0.05m}	0.077



The standardised calculation method for the life rating coefficient (a_{\rm ISO}) takes the following factors into account:

- load on the bearing
- lubrication condition
- fatigue limit of the material
- geometry of the bearing
- internal stress of the bearing
- environmental conditions

Significance of the life rating for miniature ball bearings

All standardised methods for calculating the L-10 life assume that failure is attributable to material fatigue, this type of failure occurs very rarely in miniature ball bearings. Most miniature ball bearing malfunctions are usually attributed to contamination, retainer wear or lubricant failure. Therefore L-10 life is theoretical and merely a guide. When estimating the L-10 life of a miniature ball bearing, the exact environmental conditions of the application should be considered.



Limiting speeds

Various mechanical and kinematic factors impact the maximum operational speed of a bearing. The following factors can have an effect on the limiting speed:

- Retainer load
- Noise
- Rolling kinematics
- Lubrication
- Heat generated by friction and the environment
- Inner ring slippage and radial play reduction

Retainer loading

In miniature bearings the speed limitation can be determined among other factors by the retainer material and its design.

Practical experience has shown that machined synthetic retainers are better qualified for highest speeds. These retainers generate less imbalance at high speed because of their low mass and extreme accuracy by which they are manufactured. They are characterised by higher density and elasticity enabling them to face alternating forces generated from ball acceleration and deceleration.

With more than 40 different retainer materials, our product range offers an appropriate technical solution for nearly every application.

Heat

All bearing assemblies have a maximum operating temperature, which ultimately limits the bearing speed. This maximum temperature is not only defined by the bearings mechanical components but also by the temperature range of the lubricant. In general, the operating temperature achieved at a certain speed depends on the torque generated in the bearing and the assembly's ability to transfer heat to the environment.

This assumption is the basis for calculating the thermal reference speed as noted in DIN ISO 15312.

Thermal reference speed

The thermal reference speed (n_r) defines the speed of the inner ring at which a balance is achieved between the heat generated in the bearing by torque and the heat flow dissipated through shaft and housing.

For the standardised calculation method noted in DIN ISO 15312, the following conditions apply:

- Mean ambient temperature $\vartheta_{Ar} = +20 \text{ °C}$
- Static temperature at the outer ring $\vartheta_r = +70 \text{ °C}$
- Standard bearings without seals
- 5 % of the static load rating as pure radial load
- Lubricant: mineral oil with a kinematic viscosity of $v_r = 12 \text{ mm}^2/\text{s}$ at $\vartheta_r = +70 \text{ °C}$

Significance of the thermal reference speed

The calculation of the thermal reference speed is too general and does not take into consideration application specific conditions. As such the thermal reference speed is to be used merely as guideline value allowing for direct comparison of the different bearing sizes.

Significantly higher speeds can be achieved with special modifications of the components surrounding the bearing and of the bearing itself.

By using Si_3N_4 (ceramic) balls, a highly accurate synthetic retainer, a higher bearing tolerance grade and a high-performance lubricant, significantly higher speeds can be achieved.

Elastic behaviour of deep groove radial bearings

With ball bearings two types of deformation have to be distinguished: axial and radial elastic deformation.

Axial elastic deformation

The axial elastic deformation of a ball bearing is the distance that the inner ring moves axially relative to the outer ring when the axial clearance of the ball bearing has been removed and an increasing axial load has been applied. This value does not increase linearly with increasing axial load; rather the contact ellipses between balls and raceways become larger as the load increases.

Radial elastic deformation

The radial elastic deformation is caused by a radial load component after radial clearance has been removed. Under otherwise identical conditions, with a small contact angle, the radial elastic deformation is considerably less than the axial elastic deformation. With increasing contact angle, the radial yield increases while the axial yield decreases until both values become roughly identical at approximately 35° .

Both types of deformation depend on the internal geometries of bearing, existing radial clearance and applied load.

Effect and application

A relatively large amount of yield can be reduced by using preloaded bearing pairs (see chapter "Duplexed bearings"). Preloading will result not only in a reduction of the elastic yield, resulting in increased stiffness, but also in a nearly linear relationship between loading and yield for a considerably wide range of applied loads.

For example: A ball bearing pair with a 10 N preload will maintain linearity up to approximately 30 N of applied axial load. Exceeding this load value will cause the balls to lose contact with the raceway transferring the load to one bearing.



The following formula provides an estimation of the axial preload:



Fv : axial preload [N] Fa : axial bearing load [N]

With a contact angle of 15° (C) the radial stiffness of bearing pairs is assumed to be approximately six times as high as the axial stiffness. With a contact angle of 25° (E) a factor of 2 is assumed.

Specific material properties always play an important role. In hybrid bearings using ceramic balls (e.g. Si_3N_4 , ZrO_2) the material properties of the ceramic balls should be minded. Due to the lower elasticity of the ceramic material these bearings are stiffer than bearings assembled with steel balls. The stiffness of bearings using balls made of Si_3N_4 is about 30% higher than stiffness of bearings using steel balls.

Specific applications must consider the operating temperature which can affect the bearing clearances. Likewise, differing thermal expansion coefficients may play a decisive role in bearing material selection.

For further information, please contact your nearest GRW Sales Representative.



Relationship between radial play, axial play, contact angle and tilting angle

Radial play

Radial play has a minimal effect on the quality of a bearing; however, it does have a significant effect on its performance. For example, the bearing's life rating, running noise, vibrations and thermal behavior all depend on the appropriate radial play. (See chapter: "Reduction in radial play")

Radial play is the measurement of the total movement of one ring relative to the other in a plane perpendicular to the bearing axis. In selecting the appropriate radial play the fit of the bearing on the shaft and in the housing is of particular importance.

Larger than standard radial play $(4 - 11 \mu m)$ should be selected if the ball bearing runs under axial preload and operates at high speeds, or if low torque is required.

Less than standard radial play should be specified if a radial load is applied or low noise is required.

Less than normal radial play is often specified to reduce the axial play in the application. When a very low axial play is required we recommend using duplexed bearings (see the chapter "Duplexed bearings").

In deep groove bearings there is a definite correlation between radial and axial play that is controlled by the internal geometries. For the individual radial play groupings and their respective references, refer to the chapter on "Radial play classification".

Axial play

The axial play is the measured value in which one bearing ring can move axially in relation to the other with no applied load.

Contact angle

In a load-free condition, the contact angle is called the 'nominal contact angle'. The contact angle is the angle between a plane perpendicular to the ball bearing axis and a line joining the two points where the ball makes contact with the inner and outer raceways. The contact angle of a ball bearing is determined by its radial play, as well as its inner and outer track curvatures.

The contact angle under load is called the 'operating contact angle'. Deformations of a defined size occur at the contact points between balls and raceways. The deep groove radial bearing is a relatively rigid bearing with a very small contact angle range. Here a highly accurate bearing alignment is of the utmost importance.

Tilting angle

The tilting angle of a bearing is the relative angle to which the inner and outer rings of a bearing can be tilted. The amount of tilting depends on the radial play and the internal geometries of the bearing.

Tilting of the rings should generally be avoided. Even small tilt angles of 2° or 3° may result in increased bearing noise and reduced life. It is critical to place close attention to machining tolerances of mating assembly components to assure proper bearing alignment.

Calibration of bore and outside diameters

To guarantee a uniform fit of bearings on the shaft and in the housing, it is necessary to control diameter tolerances of the bearings. It is very difficult to control very small tolerances in a production run; therefore, sorting of the rings may be necessary. Only bearings in quality grades P5 and ABEC5 or better can be sorted into groups of 2.5 µm (.0001 inch) or 1.25 µm (.00005 inch). The diameters of shaft and housing must also be accurately measured and sorted to match. For technical reasons it is not possible to supply bearings in only one specific tolerance group. This means that grading to X4, only 3 of 4 possible groups can be contained in the shipment lot, i.e. the final group distribution is subject to production machining variances.

Key to tolerance groups

					Outside diameter D											
	Tolerance fi	ield in 0.001	mm	0/-2.5	-2.5/-5	0/-1.25	-1.25/-2.5	-2.5/-3.75	-3.75/-5	0/-1	-1/-2	-2/-3	-3/-4	-4/-5		
		Tolerance fie	ld in	0/-1	-1/-2	0/5	5/-1	-1/-1.5	-1.5/-2	0/4	4/8	8/-1.2	-1.2/-1.6	-1.6/-2		ot ded
		.0001 inch	Code	1	2	А	В	С	D	E	F	G	Н	I	giù	acu
	0/-2.5	0/-1	1	11	12										10	XB
	-2.5/-5	-1/-2	2	21	22										20	ND
	0/-1.25	0/5	А			AA	AB	AC	AD						AO	
	-1.25/-2.5	5/-1	В			BA	BB	BC	BD						BO	X4B
	-2.5/-3.75	-1/-1.5	С			CA	СВ	CC	CD						CO	A4D
σ	-3.75/-5	-1.5/-2	D			DA	DB	DC	DD						DO	
Bore	0/-1	0/4	E							EE	EF	EG	EH	EI	EO	
ă	-1/-2	4/8	F							FE	FF	FG	FH	FI	FO	
	-2/-3	8/-1.2	G							GE	GF	GG	GH	GI	G0	X5B
	-3/-4	-1.2/-1.6	Н							HE	HF	HG	НН	HI	HO	
	-4/-5	-1.6/-2								IE	IF	IG	IH		10	
		not aradad		01	02	OA	OB	0C	OD	OE	OF	0G	OH	01		10
	not graded			X	(D		Xz	1D				X5D			Symbol	

Different tolerance groups are defined by grading. On the package of the ball bearing, the relevant group is indicated by means of the following code:

Examples:

Code 21:		Code B
Bore-Ø	–2.5/–5 µm	Bore-Ø
	0/–2.5 µm	Outside-Ø

SC: –1.25/–2.5 µm Ø -2.5/-3.75 µm

Method of group classification:

Bore diameter: The smallest measured diameter defines the class.



The following symbols are used for the classification of graded ball bearings:

Classification of graded bearings

Grading	in classes of 2.5 µm or .0001 inch	in classes of 1.25 µm or .00005 inch	in classes of 1 µm or .00004 inch
Bore d and outside diam D	Х	X4	Х5
Bore d only	XB	X4B	X5B
Outside diam D only	XD	X4D	X5D

Example:

SS624 P5 GPR X4B | LOO1

 $X4B = bore graded in 4 groups of 1.25 \mu m$.

The outside diameter is not graded.



Bore-Ø 0/-1.25 µm Outside-Ø not graded

Code 02:

Bore-Ø not graded Outside-Ø -2.5/-5 µm

Outer diameter: The largest measured diameter defines the class



Reduction in radial play

Ball bearing radial play can increase or decrease during operation due to external influences.

Increases in radial play can cause an increase in contact angle, which distorts the contact ellipse at the transition between raceway and shoulder. This "excessive edge loading" phenomenon may cause premature bearing failure.

In the worst case a reduction in radial play may cause excessive radial preloading of the bearing causing accelerated bearing wear and premature bearing failure.

The following factors have a direct influence on changes in radial play:

- Temperature gradients within the bearing or materials with different temperature coefficients.
- Shaft and housing fits.
- Speed related Centrifugal forces.

Reduction in radial play due to thermal expansion

Bearing clearances are set at an ambient temperature of +20 °C which excludes external loads except measuring loads. Frictional heat generation or temperature differentiation between inner and outer ring can very often cause unfavourable environments. The resulting differential expansions of inner ring and outer ring change the radial play. This factor has to be considered when designing the bearing.

$\Delta S_{PT} \approx \Delta d_{q} - \Delta d_{i} - 2\Delta D W$

- ΔS_{pT} : Change in radial play due to thermal expansion [µm]
- Δd_a : Change in outer raceway diameter for temperature T [µm]
- Δd_i : Change in inner raceway diameter for temperature T [µm]
- ΔDw : Change in ball diameter for temperature T [µm]

The resultant diameter change caused by the temperature difference is to be calculated. (Reference: ambient temperature +20 °C):

- For the outer ring: $\Delta d_{\alpha} = d_{\alpha 0} \cdot \alpha \cdot \Delta T$
- For the inner ring: $\Delta d_i = d_{i0} \cdot \alpha \cdot \Delta T$
- For the balls: $\Delta Dw = Dw \cdot \alpha \cdot \Delta T$
- d_{a0} : Raceway diameter of outer ring at +20 °C [mm]
- d_{io} : Raceway diameter of inner ring at +20 °C [mm]
- Dw : Ball diameter at +20 °C [mm]
- α : Linear expansion coefficient [K⁻¹] for 100Cr6 ... 11 · 10⁻⁶ X65Cr13 ... 10.8 · 10⁻⁶ X30CrMoN15-1 ... 10.8 · 10⁻⁶ Si₃N₄... 3.2 · 10⁻⁶ ZrO₂ ... 10.0 · 10⁻⁶
- ΔT : Temperature difference between temperature T and ambient temperature of +20 °C in [K]

Reduction in radial play due to interference fit

Interference fits cause a reduction in radial play and so the fitting tolerances should be chosen carefully. The reduction in radial play depends on the effective interference fit and the ring thickness ratio. These ratios can be calculated as follows:

$\Delta S_{\text{RII}} \approx \mathbf{k} \cdot \ddot{\mathbf{u}}$

- $\Delta S_{\text{\tiny RII}}$: Reduction in radial clearance due to interference fit [µm]
- : Factor given in the table on the next page, taking for granted that inner ring is pressed onto a complete shaft or outer ring is pressed into a stable, non-deformable housing.
- ü : Largest interference fit [µm]

If interference fits are used on the shaft and on the housing, the total reduction in radial play is determined by adding both values.

k-factor for inner ring (IR) and outer ring (OR)

motric

Basic symbols	IR	AR	Basic symbols	IR	AR	Basic sym- bols	IR	AR
68/1,5/0003	0.4	0.8	694	0.7	0.8	699	0.7	0.8
681	0.6	0.8	604	0.6	0.8	609	0.7	0.8
691	0.5	0.8	624	0.6	0.8	629	0.6	0.8
68/1,5/0001	0.5	0.8	634*	0.5	0.8	6800	0.8	0.9
68/1,5	0.8	0.8	675	0.9	0.9	6900	0.8	0.9
69/1,5	0.5	0.8	675/004	0.9	0.9	6000	0.7	0.8
682	0.7	0.8	694/1002	0.9	0.8	6901	0.8	0.9
682/005	0.7	0.8	685	0.8	0.8	6001	0.7	0.9
692/003	0.6	0.8	685/003	0.8	0.8	6001/003	0.7	0.9
692	0.6	0.8	695	0.7	0.8	6802	0.9	0.9
693/0001	0.5	0.9	605	0.6	0.8	6902	0.8	0.9
67/2,35	0.8	0.8	625	0.6	0.8	6002	0.8	0.9
68/2,35	0.8	0.9	635	0.5	0.8	6803	0.9	0.9
67/2,5	0.8	0.9	676/003	0.9	0.9	6903	0.8	0.9
68/2,5	0.7	0.9	695/1202	0.8	0.9	6003	0.8	0.9
69/2,5	0.6	0.9	686	0.8	0.9	6804	0.9	0.9
683/0001	0.6	0.9	696	0.7	0.8	6904	0.8	0.9
60/2,5	0.6	0.8	625/0002	0.7	0.8	6805	0.9	0.9
673	0.8	0.9	626	0.6	0.8			
683	0.8	0.9	688A/1322	0.8	0.9			
683/003	0.8	0.9	687	0.8	0.9			
693/003	0.7	0.9	697	0.7	0.8			
693	0.7	0.9	607	0.7	0.8			
683/8	0.8	0.8	627	0.6	0.8			
623	0.6	0.8	688A/142	0.9	0.8			
623/13	0.6	0.6	688	0.8	0.9			
633	0.5	0.8	688/003	0.8	0.9			
674	0.9	0.9	698	0.7	0.8			
684	0.8	0.9	608	0.7	0.8			
684/103	0.8	0.8	689	0.8	0.9			
684/10	0.8	0.8	689/003	0.8	0.9			

Subject to change due to technical improvement.



inch

Basic symbols	IR	AR
1016	0.7	0.8
1191	0.6	0.8
1397	0.6	0.8
5/64	0.6	0.8
2380	0.8	0.9
3/32	0.5	0.9
3175/0002	0.6	0.9
3175	0.8	0.9
1/8A	0.7	0.9
3175/6	0.8	0.6
1/8A/6	0.7	0.7
1/8B	0.6	0.9
3175/55	0.8	0.5
3175/6	0.8	0.6
3175/8	0.8	0.4
1/8B/083	0.6	0.6
3967	0.7	0.9
4763A	0.9	0.9
4763B	0.8	0.9
4763A/082	0.9	0.6
4763B/083	0.8	0.7
3/16	0.7	0.9
6350A	0.9	0.9
6350B	0.8	0.9
1/4A	0.7	0.8
1/4	0.6	0.8
7938	0.9	0.9
3/8	0.7	0.8
12700B	0.9	0.9
1/2	0.7	0.8
1/2/001	0.7	0.8

* For a detailed example, refer to page 22.



Reduction in radial play

Reduction in radial play due to centrifugal forces

At very high shaft speeds or inner ring rotation the centrifugal forces of the rotating parts increase. The load on the outer ring and the balls also increases and the inner ring expands. The expansion of the inner ring changes the fit of the shaft and bearing. The bearing may begin to slip on the shaft. In this situation, a tighter fit must be selected.

These types of deformations depend on bearing size, retainer, balls, materials used and inner geometry of the bearing.

Please contact our sales engineers to find out more about the reduction in radial play due to centrifugal forces.

Example:

The ball bearing SS634-2Z GPR \mid (d = 4 mm, D = 16 mm, Dw = 2.50 mm, material of rings and balls: X65Cr13) is to run in an application at 35,000 1/min. During the operating phase the temperature at the inner ring is +60 °C and at the outer ring +30 °C. The ball bearing is mounted on the shaft with a press fit j5 (+3/-2) and in the housing with a tight fit K5 (+2/-6).

Change in radial clearance due to thermal expansion:

Outer ring:

 $d_{a0} \approx (d+D)/2 + Dw = (4+16) \text{ mm}/2 + 2.50 \text{ mm}$ = 12.50 mm $\Delta d_{\alpha} \approx d_{\alpha 0} \cdot \alpha \cdot \Delta T = 12.50 \text{ mm} \cdot 10.8 \cdot 10^{-6} \text{ } 1/\text{K} \cdot 10^{-6} \text{ }$ 10 K = 1.35 µmInner ring: $d_{i0} \approx (d+D)/2 - Dw = (4+16) \text{ mm}/2 - 2.50 \text{ mm}$ $= 7.50 \, \text{mm}$ $\Delta d_{i} \approx d_{i0} \cdot \alpha \cdot \Delta T = 7.50 \text{ mm} \cdot 10.8 \cdot 10^{-6} \text{ } 1/\text{K}$ $\cdot 40 \text{K} = 3.24 \, \mu \text{m}$ Ball:

Dw = 2.50 mm

 $\Delta Dw \approx Dw \cdot \alpha \cdot \Delta T = 2.50 \text{ mm} \cdot 10.8 \cdot 10^{-6} \text{ } 1/\text{K} \cdot$ (10+40) K/2 ≈ 0.68 µm

Change in radial clearance due to thermal expansion:

 $\Delta S_{PT} \approx \Delta d_{a} - d_{i0} - 2\Delta Dw$ $\Delta S_{\text{PT}} \approx (1.35 - 3.24 - 2 \cdot 0.68) \, \mu\text{m} = -3.25 \, \mu\text{m}$

The radial clearance is reduced due to the temperature difference between inner ring and outer ring by 3.25 µm.

Change in radial clearance due to interference fit:

Outer ring:

Outside diameter: 0/-8 µm Housing diameter: +2/-6 µm $\rightarrow \ddot{u} = 6 \mu m$ $\Delta S_{R\ddot{U}a} \approx k \cdot \ddot{u}$ $\Delta S_{RU_{q}}^{nod} \approx 0.8 \cdot 6 \ \mu m = 4.8 \ \mu m$

Inner ring:

Bore: $0/-8 \mu m$ Shaft: $+3/-2 \mu m$ →ü = llµm $\Delta S_{R\ddot{i}i} \approx k \cdot \ddot{u}$ $\Delta S_{\text{RU}} \approx 0.5 \cdot 11 \,\mu\text{m} = 5.5 \,\mu\text{m}$ The radial clearance changes due to the interference fit by $4.8 \ \mu m + 5.5 \ \mu m = 10.3 \ \mu m$

Total change of radial clearance due to thermal expansion and interference fit:

 $\Delta S_{P} = \Delta S_{PT} + \Delta S_{PII} [\mu m]$ $\Delta S_{P} = 3.25 \ \mu m + 10.3 \ \mu m = 13.55 \ \mu m$

This total reduction in radial clearance must be considered when selecting the radial clearance of the bearing.

Radial play classification

Radial bearing clearance for deep groove radial bearing

d	max 6 mm	
C2	O to 6 µm	
CN	4 to 11 µm	
C3	10 to 20 µm	
C4	14 to 20 μm	
C5	18 to 28 µm	

more than 6 to 10 mm d

C2	0 to 6 µm
CN	4 to 11 µm
С3	10 to 20 µm
C4	14 to 29 µm
С5	20 to 37 µm

more than 10 to 18 mm d

22	0 to 9 µm
	3 to 18 µm
23	11 to 25 µm
24	18 to 33 µm
25	25 to 45 µm

more than 18 to 24 mm d

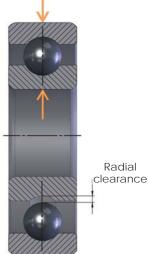
C2	0 to 10 µm
CN	5 to 20 µm
C3	13 to 28 µm
C4	20 to 36 µm
С5	28 to 48 µm

The regular radial clearance is not indicated in the ball bearing numbering system.

Deviating	radial	clearance	data
metric sys	stem		

C1/5	1 to 5 µm
C4/8	4 to 8 µm
C7/11	7 to 11 µm
C10/15	10 to 15 µm





d more than 24 to 30 mm

C2]	to 11 µm
CN	5	to 20 µm
C3	13	to 28 µm
C4	23	to 41 µm

C5 30 to 53 µm

d more than 30 to 40 mm

C2	1	to 11 µm
CN	6	to 20 µm
C3	15	to 33 µm
C4	28	to 46 µm
C5	40	to 64 µm

d more than 40 to 50 mm

C2	1	to	11	μm
CN	6	to	23	μm
C3	18	to	36	μm
C4	30	to	51	μm
C5	45	to	73	μm

Deviating radial clearance data inch system

KO2 0" to .0002" K13 .0001" to .0003" K24 .0002" to .0004" .0003" to .0005" K35 .0004" to .0006" K46 K.58 .0005" to .0008"



The functional tests

There are different functional testings that can be performed by GRW. As a standard 100% of our ball bearings are noise tested. The following tests are also available: axial vibration test, torque test, preload measurement.

These tests ensure the uniformity of the production run and compliance with customer requirements. All functional tests carried out by GRW take place in a class 10,000 clean room (ISO 14644-1).

The functional test method is always selected to simulate the intended use of the bearing.

Noise test GPR

In the GRW numbering system GPR designates 100% noise testing. Using highly sensitive noise testing equipment, the amplitude of the vibrations generated by the miniature bearings is measured at specified speed and frequencies. This method detects imperfections, such as ball or raceway failures and isolates their root cause.

The noise test is carried out in a class 10,000 clean room in accordance with ISO 14644-1. A Standard reference oil is used to eliminate the variable effects of different lubricants.

Axial vibration test GPA

GPA stands for noise testing in the axial direction. Similar to the GPR test, the axial vibrations measured by the GPA vibration meter identify the shape and surface properties of raceways and balls in the bearings.

GPA testing measures vibration noise in four distinct frequency ranges as compared to two frequency ranges for the GPR test. The amount of movement or 'peak to peak displacement' value is also recorded. The cumulative total of these distinct measurements provides a direct understanding of the ball bearing's running behaviour.

As with the GPR test, standard reference oil is used to eliminate the variable effects of different lubricants.

The GPA test is offered at an additional charge. If you require any further information, please contact a GRW sales representative.

Torque test

higher speeds.

GRW uses different methods to measure starting and dynamic torque. The Asch testing device due to MIL-STD-206 provides very exact and reliable starting torque values. During this test the outer ring is driven and the inner ring is loaded relative to each bearing size. The standard axial loading of the inner ring is 75 g for ball bearings with an outer diameter of up to 10 mm. Ball bearings with a larger outer diameter (> 10 mm) are loaded with 400 g.

Since there is no universally accepted standard for torque measurement, the torques of identical bearings can only be compared if they have been measured under the same measuring conditions with the same measuring devices.

Table "Maximum starting torque in μ Nm" shows reference values for the maximum starting torque. These values apply for instrument ball bearings without seals, P5 or ABEC5 or better, which are lubricated with instrument oil having a low viscosity $\leq 14 \text{ mm}^2/\text{s}$ at +40 °C. The values can be 10 to 40 times higher for ball bearings with grease lubrication. Running or dynamic torque is the force required to keep a bearing in rotation. A special dynamic torque tester developed by GRW for this very purpose is available on request to measure the running torque at

Maximum starting torque in µNm

Basic symbols	Torque in [µNm]	Load in [g]	Basic symbols	Torque in [µNm]	Load in [g]	Basic symbols	Torque in [µNm]	Load in [g]
681	15	75	695	69	400	1016	15	75
691	15	75	605	69	400	1191	15	75
68/1,5	15	75	625	69	400	1397	15	75
69/1,5	15	75	635	76	400	5/64	15	75
682	15	75	686	69	400	2380	15	75
692	15	75	696	69	400	3/32	15	75
67/2,35	15	75	626	76	400	3175	15	75
68/2,35	15	75	687	69	400	1/8A	15	75
68/2,5	15	75	697	76	400	1/8B	16	75
69/2,5	15	75	607	76	400	3967	15	75
60/2,5	16	75	627	80	400	4763A	15	75
673	16	75	688A	52	400	4763B	16	75
683	16	75	688	76	400	3/16	52	400
693	16	75	698	76	400	6350A	15	75
623	16	75	608	80	400	6350B	52	400
674	16	75	689	76	400	1/4A	60	400
684	16	75	699	80	400	1/4	70	400
694	65	400	609	80	400	7938	52	400
604	65	400	629	100	400	3/8	95	400
624	69	400	6800	80	400			
634	69	400	6900	95	400	_		
675	65	400	6000	100	400			
685	65	400						

Comparison of measuring units

	1 μNm =	1 cmp =	1 oz.in. =	1 cNcm =
μNm]	100	7200	100
cmp	0.01]	72]
oz.in.	0.000139	0.0139]	0.0139
cNcm	0.01]	72]

Assembly of low-torque ball bearings

Shaft and housing fits and tolerances for low-torque bearings are particularly important. Shaft and housing tolerances need to be selected so that they result in a sliding fit. Please refer to the chapters "Fitting Tolerances" and, "Reduction in radial play".

Even a small misalignment of the inner or outer ring can result in increased bearing torque. Particular attention must be given to the exact alignment between shaft and housing bore as well as to the parallelism of the mating faces.

Extreme cleanliness of parts and assembly area is essential to produce a perfect low-torque

bearing. Even tiniest contaminations of the ball bearings can cause torque peaks, which may be many times higher than the average torque level.

Preloading test

Another testing device specifically developed by GRW measures and records the preloading of duplexed bearings (following the "broken curve" method). This type of measurement is available on request.



Tolerance and runout tables – inner ring

national Organization for Standardisation) and ABEC bearings according to ABEC quality standards ABEC1 standards (Annular Bearing Engineering Committee). to ABEC9 (ABEC9 = highest tolerance). For metric size bearings, tolerances comply with ISO

GRW bearings conform to the applicable ISO (Inter- quality PO to P2 (P2 = highest tolerance). For inch size

GRW manufactures miniature ball bearings accord- GRW's sales engineers will be happy to help you ing to the highest quality standards for both inch and choosing the suitable quality for your application, including tolerances of mating parts, such as shafts and metric sizes. housings, to create a bearing friendly environment.

Definition:		Diameter	d [mm]		ΡΟ [μm]	P6 [µm]		P5 P4 Im] [µm]		P5A ⁽⁴⁾ [µm]	P4A (4) [µm]	P4S (5) [µm]		BEC 1 01 inch]	ABE (ABEC [.0001 i		ABEC7 [.0001 incl		BEC9 01 inch]		C3P 1 inch]	ABEC [.0001 i		ABEC7 [.0001 in		ABEC9P 0001 inch]		C5T (6) 01 inch]
		series	above	to max	ι. min.	max. min.	. max.	min. max.	min. max. mi	n. max. min	. max. min	. max. min.	max.	min.	max.	min.	max.	min.	max. mi	n. max	. min.	max.	min.	max.	min.	max. r	nin. m	ax. min	. max.	min.
ingle plane mean			0.6	18 0	-8	0 -7	0	-5 0	-4 0 -2.	50-5	50-4	0 -4	0	-3	0	-3	0	-2	0 -1.	5 0	-]	0	-2	0	-2	0	-2 0) -]	0	-2
ore diameter	∆dmp		18	30 0	-10	0 -8	0	-6 0	-5 0 -2.	50-6	50 -5	0 -5	0	-4	0	-3	0 -	-2.5	0 -	2 0	-]	0	-2	0	-2	0	-2 0) -]	0	-2
eviation			30	50 0	-12	0 -10	0	-8 0	-6 0 -2.	5		0 -6	0	-4.5	0	-4	0	-3	0 -2.	5 0	-]								0	-3
			0.6	18 10		9	5	4	2.5	3	2.5	2.5												1		1		5		
		7/8/9	18	30 13		10	6	5	2.5	3	2.5	2.5												1		1		5		
			30	50 15		13	8	6	2.5			2.5																		
ore diameter variation			0.6	18 8		7	4	3	2.5	3	2.5	2.5												1		1		5		
n a single radial plane	Vdsp	0	18	30 10		8	5	4	2.5	3	2.5	2.5												1		1		5		
out of roundness)			30	50 12		10	6	5	2.5			2.5																		
			0.6	18 6		5	4	3	2.5	3	2.5	2.5												1		1		5		
		2/3		30 8		6	5	4	2.5	3	2.5	2.5												1		1		5		
			30	50 9		8	6	5	2.5			2.5																		
A 1 10 .			0.6	18 6		5	3	2	1.5	3	2	1.5												1		1		5		
Aean bore diameter ariation (conicity)	Vdmp		18	30 8		6	3	2.5	1.5	3	2.5	1.5												1		1		5		
			30	50 9		8	4	3	1.5			1.5																		
			0.6 2	2.5 0	-40	0 -40	0	-40 0	-40 0 -4	0 0 -25	5 0 -25	0 -100																		
			0.6	10									0	-50	0	-50	0	-16	0 -10	5 0	-16	0	-50	0	-10	0 -	10 0	-10)	
ariation of a single nner ring width from	$\Delta Bs^{(1)}$		2.5	10 0	-120	0 -120	0	-40 0	-40 0 -4	0 0 -25	5 0 -25	0 -100																	-	
ominal dimension	7 D 3		10	18 0	-120	0 -120	0	-80 0	-80 0 -8	0 0 -25	5 0 -25	0 -100	0	-50	0	-50	0	-32	0 -32	2 0	-32	0	-50	0	-10	0 -	10 0	-10	0	-10
			18	30 0	-120	0 -120	0	-120 0 -	20 0 -12	0 0 -25	5 0 -25	0 -120	0	-50	0	-50	0	-50	0 -50	0 (-50	0	-50	0	-10	0 -	10 0) -1C	0	-10
			30	50 0	-120	0 -120	0	-120 0 -	20 0 -12	0		0 -120	0	-50	0	-50	0	-50	0 -50) ()	-50				/				0	-50
			0.6 2	2.5 12		12	5	2.5	1.5			1.5												/					- martin	
			0.6	10									6		6		2		1	.5				2		1		5		
ariation in width	VBs		2.5	10 15		15	5	2.5	1.5	5	2.5	1.5											11							
of the inner ring	V DS		10	18 20		20	5	2.5	1.5	5	2.5	1.5	8		8		2		1	.5		1		2		1		5	2	
			18	30 20		20	5	2.5	1.5	5	2.5	1.5	8		8		2		1	.5		11		2	1	1		5	2	
			30	50 20		20	5	3	1.5			1.5	8		8		2]	.5	1			1					2	
			0.6 2	2.5 10	T	5	4	2.5	1.5	3.5	2.5	1.5	3		2.5		1.5	T	1	.5		2		1.5		1		5	AT SA	
adial runout of				10 10		6	4	2.5	1.5	3.5	2.5	1.5	3		2.5		1.5		1	.5		2		1.5		1	1	5		AA
nner ring in assembled bearing	Kia			18 10		7	4	2.5	1.5	3.5	2.5	1.5	4		3		1.5		1	.5		2	1	1.5		1	250	5	2	X
dynamic imbalance)				30 13		8	4	3	2.5	3.5	3	2.5	5		3		1.5		1	1		3		1.5		1.5	KN	XX	2	XX
			30	50 15		10	5	4	2.5			2.5	6		4		2		1.5	N						A	J-X	JARX	3	
			0.6	18			7	3	1.5	7	3	1.5					3		1	.5		A		3	12	KPA	-CX	5	3	
ace runout with bore ateral runout)	Sd		18	30			8	4	1.5	8	4	1.5					3		1.5	.5				3	10.1	1.5	XX	5	3	
			30	50			8	4	1.5			1.5					3		1.5	.5				ARI	20	HXX	Y		3	
Assembled bearing inner			0.6	18			7	3	1.5	7	3	1.5					3		1	.5				3 00/	T	XX	· ·	5	3	
ing face runout with	Sia		18	30			8	4	2.5	8	4	2.5					3		1.5	1				3	77	1.5		5	3	
aceway (axial runout)				50			8	1	2.5			2.5					3		1.5	1				ANY	12	Y			3	

Subject to change due to technical improvement.

⁽¹⁾ Tolerance for matched bearings is 0/-200 µm
 ⁽²⁾ Applicable before assembly of bearing and after removal of the inner and/ or outer circlips

⁽³⁾ For flanged ball bearings the inner side of the flange

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⁽⁴⁾ For deep groove radial bearings only
 ⁽⁵⁾ For spindle ball bearings only
 ⁽⁶⁾ Nominal value for bores of 9 mm and bigger





Tolerance and runout tables – outer ring

Definition:		Diameter	D [mm]		PO [µm]		P6 [µm]	P : [pr		P4 [µm]		P2 [µm]	Ρ5Α [μm]		P4A ([µm]		P4S (5))		BEC1 D1 inch]		SEC3		BEC5 01 inch]		BEC7 01 inch]		BEC9 01 inch]		EC3P		EC5P		EC7P D1 inch]	ABE [.0001		ABEC5 [.0001 ir	
		series	above									ıx. min.			nax. n		nax. mi	n.	max.	min.	max.	min.	max.						max.	-	max.		max.	-	max.	-	max.	-
ingle plane mean utside diameter leviation	∆Dmp		30	18 0 30 0 50 0 80 0	_(-]	8 0 7 0 1 0 3 0	-7 -8 -9 -11	0	-5 (-6 (-7 (-9 (0	-4 0 -5 0 -6 0 -7 0		0 0 0	-5 (-6 (-7 ()	-4 (-5 (-6 () .	-4 -5 -6 -7	0 0 0 0	-3 -4 -5 -5	0 0 0 0	-3 -3 -4 -4.5	0 0 0 0	-: -: -3	3 0	-2 -2 -2.5 -3	0 0	-1 -1.5 -1.5 -1.5	0 0 0	-3 -3 -3	0	-2 -2 -2	0 0 0	-2 -2 -2	0 0 0	-1 -1.5 -1.5	0 0 0	-2 -4 -4
		7/8/9	18 30	50 1	2	9 10 11 14		5 6 7 9	2 (-	4 5 6 7	2.5 4 4 4	5	3 3 3	2	2.5 2.5 2.5	4	2.5 4 4 4]]]]]]		.5 .8 .8			
Dutside diameter ariation in a single adial plane put of roundness)	VDsp ^[2]	0	18 30	18 8 30 9 50 1 80 1	1	7 8 9 11		4 5 5 7		3 4 5 5	2.4 4 4 4	5	3 3 3	2	2.5 2.5 2.5		2.5 4 4 4]]]		1 1 1		.5 .8 .8			
		2/3	18 30	18 6 30 7 50 8 80 1		5 6 7 8		4 5 5 7		3 4 5 5	2.5 4 4 4	5	3 3 3	2	2.5 2.5 2.5		2.5 4 4 4]]]]]]		.5 .8 .8			
Nean outside iameter variation conicity)	VDmp ^[2]		18 30	18 6 30 7 50 8 80 1	0	5 6 7 8		3 3 4 5		2 2.5 3 3.5	1.5 2 2 2	5	3 3 4		2 2.5 3		1.5 2 2 2]]]]]]		.5 .8 .8			
ariation of a single uter ring width from ominal dimension	$\Delta Cs^{[1]}$		30	18 30 50 80	identi	cal wit	h ∆ Bs fo	or inne	r ring o	the sar	me bea	ring		-25 (-25 (-25 (-25 () -12) -12) -15	0	0 0 0	-50 -50 -60	0 0 0	-50 -50 -60	0 0 0	-51 -51 -61	0 0	-50 -50 -60	0	-50 -50 -60	0 0	-50 -50	0 0	-10 -10	0 0	-10 -10	0 0	-10 -10	0	-10 -10 -50
ariation in width	VCs		18 30 50	18 30 50 80		cal wit	th VBs fo	or inner	r ring of	the sar	me bea	ring	5 5		2.5 2.5		1.5 1.5 1.5		8 8 10		8 8 10		2 2 2.5		1 1 1		.5 .5 .5				2 2		1		.5 .5		2 2 2	
tadial runout of outer ring in ussembled bearing dynamic imbalance)	Kea		18 30	18 1 30 1 50 2 80 2	5 0	8 9 10 13		5 6 7 8		3 4 5 5	1.5 2.5 2.5 4	5	5 6 7	2	3 4 5		1.5 2.5 2.5 4		6 6 8 10		4 4 5		2 2 3 3		1.5 1.5 2 2		.5 1 1 1.5		4 4 4		2 2 2	/	1.5 1.5 2		.5 1 1		2 3 3	
'ariation of outside urface generatrix nclination with face ³⁾ ateral runout)	SD			80				8	4	4	1.5	5	8	2	4		1.5						3		1.5		.5			/	3		1.5		.5		3	
ssembled bearing oute ng face flange back ace rounout with racew axial runout)	Sea Way		18 30 50	18 30 50 80				8 8 8 10		5 5 5 5	1.4 2.4 2.4	5 5	8 8 8		5 5 5		1.5 2.5 2.5 4						3 3 3 5		2 2 2 2		.5 1 1 1.5				3 3 3		2 2 2		.5 1 1		3 3 4	
ssembled bearing oute ng face flange back ace runout in the ssembled bearing	er Seal		18 30 50	18 30 50 80				11 11 11 11		7 7 7 7	3 4 4		10 10 10	7	7 7 7																3 3 3		3 3 3	XE	S.			
ariation of a single utside diameter f outer ring ange diameter is sed for positioning	∆FD		10 18 30	10 0 18 0 30 0 50 0 80 0	-4 -5 -6	5 0 3 0 2 0 2 0 4 0	-36 -43 -52 -62 -74	0 0 0 0	-36 (-43 (-52 (-62 (-74 (((36 0 43 0 52 0 62 0 74	-43 -52	0	-25 () -25 () -25 () -25 ()) -) -	-25 -25 -25 -25													50 50 50 50	-20 -20 -20 -20	0 0 0	-10 -10 -10 -10	0000	-10 -10 -10 -10			XX	X
'ariation of a single vidth outer ring flange rom nominal dimension	∆ FB		2.5 10 18 30	10 0 18 0 30 0 50 0 80 0	-120 -120 -120 -120		-120 -120 -120 -120 -120	0 0 0 0	-40 (-80 (-120 (-120 (-120 (C - C - C - 1 - C	40 0 80 0 20 0 20 0 20 0	-80 -120	0 0	-40 (-50 (-50 (-50 () -) -	-40 -50 -50 -50										A			0 0 0 0	-20 -20 -20 -20		-20 -20 -20 -20	0000	-20 -20 -20 -20 -20				

Subject to change due to technical improvement. ⁽¹⁾ Tolerance for matched bearings is 0/-200 µm
 ⁽²⁾ Applicable before assembly of bearing and after removal of the inner and/ or outer circlips

⁽³⁾ For flanged ball bearings the inner side of the flange
 ⁽⁴⁾ For deep groove radial bearings only
 ⁽⁵⁾ For spindle ball bearings only
 ⁽⁶⁾ Nominal value for bores of 9 mm and bigger

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GRW-	Main di	mensions in	Bearin	ng without clos	ure in [mm]	[inch]	Bear	ring with clos	ure in [mm]	[inch]	Chamfer in		on dimensions		ngs acc. to	Closure v	variants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
designation		nm] nch]	Width without closure	Width with extended inner ring		imensions closure	extended inner ring	Width with extended inner ring		imensions closure	[mm] [inch]	[r	DIN 5418 nm] nch]	DIN ISC) ^[2] (max)				
				without closure			with closure	with closure				Shaft diameter	Housing diameter						
Basic symbols	d	D	В	B1	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} ⁽¹⁾	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
67/0,6	0.60	2.00	0.80	-	-	-	-	-	-	-	0.05	1.00	1.60	27	7	-	-	170,000	-
	.0236	.0787	.0315								.002	.039	.063						
68/1,5/0003	0.80	4.00	2.00	-	5.00	0.60	2.00	-	5.00	0.60	0.05	1.20	3.60	163	44	Х	-	138,000	-
	.0315	.1575	.0787		.1969	.0236	.0787		.1969	.0236	.002	.047	.142					150.000	
681	1.00	3.00	1.00	-	-	-	2.00	-	-	-	0.05	1.40	2.60	82	22	Х	-	150,000	-
	.0394	.1181	.0394				.0787				.002	.055	.102	50	01	V		170.000	
681/003	1.00	3.00	2.00	-	-	-	2.00 .0787	-	-	-	0.05	1.40	2.60	52	21	Х	-	170,000	-
691	.0394 1.00	.1181 4.00	.0787 1.60	-	-	_	2.30	_	-	-	.002 0.10	.055 1.60	.102 3.40	160	43	_	_	126,000	
091	.0394	.1575	.0630	-	-	-	.0906	-	-	-	.004	.063	.130	100	43	_	_	120,000	-
68/1,5/0001	1.00	4.00	.0030	-	-	-	2.00	-	5.00	0.60	0.05	1.40	3.60	163	44	X	_	130,000	_
00/ 1,0/ 0001	.0394	.1575	_				.0787		.1969	.0236	.002	.055	.142	100		~		130,000	
68/1,5/0011	1.00	4.00	2.00	-	5.00	0.60	2.00	-	-	-	0.05	1.40	3.60	163	44	Х	_	130,000	_
00, 1,0, 0011	.0394	.1575	.0787		.1969	.0236	.0787				.002	.055	.142	100				,	
68/1,5	1.50	4.00	1.20	2.00	5.00	0.40	2.00	-	5.00	0.60	0.05	1.90	3.60	163	44	Х	-	153,000	_
	.0591	.1575	.0472	.0787	.1969	.0157	.0787		.1969	.0236	.002	.075	.142					, ,	
68/1,5A	1.50	4.00	-	-	-	-	2.00	-	5.00	0.60	0.05	2.10	3.60	112	33	Х	-	120,000	_
	.0591	.1575	.0787				.0787		.1969	.0236	.002	.083	.142						
69/1,5 (4)	1.50	5.00	2.00	2.80	6.50	0.60	2.60	3.40	6.50	0.80	0.15	2.30	4.20	192	59	Х	-	109,000	-
	.0591	.1969	.0787	.1102	.2559	.0236	.1024	.130	.2559	.0315	.006	.091	.165						
69/1,5/002	1.50	5.00	-	-	-	-	2.00	-	6.50	0.60	0.15	2.30	4.20	192	59	X		93,000	_
	.0591	.1969					.0787		.2559	.0236	.006	.091	.165					and the second sec	7
60/1,5	1.50	6.00	2.50	-	7.50	0.60	3.00	-	7.50	0.80	0.15	2.30	5.20	330	98	Х	-	90,000	-
	.0591	.2362	.0984		.2953	.0236	.1181		.2953	.0315	.006	.091	.205						
672	2.00	4.00	1.20	-	-	-	2.00	-	-	-	0.05	2.40	3.60	124	40	Х	-	104,000	
	.0787	.1575	.0472				.0787				.002	.094	.142		11/1				
682	2.00	5.0	1.50	2.30	6.10	0.50	2.30	3.10	6.10	0.60	0.08	2.50	4.50	192	59	Х	Х	116,000	71,000
	.0787	.1969	.0591	.0906	.2402	.0197	.0906	.122	.2402	.0236	.003	.098	.177						
682/003	2.00	5.00	-	-	-	-	2.50	-	6.20	0.60	0.10	2.60	4.40	169	50	Х		100,000	XXXX
	.0787	.1969					.0984		.2441	.0236	.004	.102	.173	DE			Æ	KNX	YYYY
682/005	2.00	5.00	2.60	-	6.50	0.80	2.60	-	6.50	0.80	0.08	2.50	4.50	192	59	Х	-	105,000	-
	.0787	.1969	.1024		.2559	.0315	.1024		.2559	.0315	.003	.098	.177	1000	- M			NIE	
692/003	2.00	6.00	2.00	-	-	-	-	-	-	-	0.15	2.80	5.20	286	90	- /	ALL'S	91,000	-
	.0787	.2362	.0787								.006	.110	.205	Magaz		AND	XHAN	J.	
692	2.00	6.00	2.30	3.10	7.50	0.60	2.30	3.10	7.50	0.60	0.15	2.80	5.20	286	90	Х	Х	91,000	65,000
	.0787	.2362	.0906	.1220	.2953	.0236	.0906	.122	.2953	.0236	.006	.110	.205						

Note:

⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius.
⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer.
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GRW-		mensions in	Bearin	ng without clos	ure in [mm]	[inch]	Bea	ring with clos	ure in [mm]	[inch]	Chamfer in		on dimensions		ngs acc. to	Closure v	ariants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
designation		nm] nch]	Width without closure	Width with extended inner ring	Flange d without	imensions closure	Width with extended inner ring	Width with extended inner ring	Flange d with c	imensions closure	[mm] [inch]	[r	DIN 5418 nm] nch]	DIN ISC) ^[2] (max)				
				without closure		1		with closure		1		Shaft diameter	Housing diameter		I		I		L
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	$d_{\mathfrak{a}min}$	D _{a max}	C, [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
692/005	2.00	6.00	2.50	-	7.20	0.60	2.50	-	-	-	0.15	2.80	5.20	330	99	Х	-	90,000	-
	.0787	.2362	.0984		.2835	.0236	.0984				.006	.110	.205						
692/004	2.00	6.00	3.00	-	7.50	0.80	3.00	-	7.50	0.80	0.15	2.80	5.20	330	99	Х	-	95,000	-
	.0787	.2362	.1181		.2953	.0315	.1181		.2953	.0315	.006	.110	.205						
683/0003	2.00	7.00	3.00	-	8.20	0.60	3.00	-	8.20	0.60	0.15	2.80	6.20	386	129	Х	-	75,000	-
	.0787	.2756	.1181		.3228	.0236	.1181		.3228	.0236	.006	.110	.244						
693/0001	2.00	8.00	4.00	-	9.50	0.90	4.00	-	9.50	0.90	0.15	2.80	7.20	644	215	Х	-	67,000	-
	.0787	.3150	.1575		.3740	.0354	.1575		.3740	.0354	.006	.150	.283						
67/2,35	2.35	5.00	1.50	2.30	6.10	0.50	2.30	-	6.10	0.60	0.08	2.50	4.50	192	59	Х	-	120,000	-
	.0925	.1969	.0591	.0906	.2402	.0197	.0906		.2402	.0236	.003	.098	.177						
68/2,35	2.35	5.50	2.00	-	-	-	-	-	-	-	0.08	2.90	5.00	286	90	-	-	91,000	-
	.0925	.2165	.0787								.003	.114	.197						
67/2,5	2.50	5.00	1.50	-	-	-	-	-	-	-	0.08	2.90	4.60	192	59	-	-	93,000	-
	.0984	.1969	.0591								.003	.114	.181						
68/2,5	2.50	6.00	1.80	2.60	7.10	0.50	2.60	3.40	7.10	0.80	0.08	3.00	5.50	286	90	Х	Х	101,000	61,000
	.0984	.2362	.0709	.1024	.2795	.0197	.1024	.1303	.2795	.0315	.003	.118	.217						
69/2,5/002	2.50	7.00	-	-	-	-	2.50	-	-	-	0.10	3.10	6.40	177	58	Х	-	75,000	
/	.0984	.2756					.0984				.004	.122	.252						17778
69/2,5	2.50	7.00	2.50	-	8.50	0.70	3.50	-	8.50	0.90	0.15	3.30	6.30	432	149	Х	Х	87,000	53,000
(.0984	.2756	.0984		.3346	.0276	.1307		.3346	.0354	.006	.130	.248	100	1.40	Y			
683/0001	2.50	7.00	2.00	-	8.10	0.50	3.00	-	8.10	0.80	0.10	3.60	6.40	432	149	X		88,000	Constanting of the second
10/05	.0984	.2756	.0787	0.40	.3189	.0197	.1181	0.40	.3189	.0315	.004	.142	.252	400	1.40	V	V	01.000	52.000
60/2,5	2.50	8.00 .3150	2.80	3.60	9.50 .3740	0.70	2.80	3.60	9.50	0.70	0.15	3.30	7.20 .283	432	149	Х	Х	81,000	53,000
40/0 E/004	.0984					.0276	.1102		.3740	.0276	.006	.130		E E O	177	V		71.000	
60/2,5/004	2.50 .0984	8.00 .3150	4.00 .1575	-	9.50 .3740	0.90 .0354	4.00 .1575	-	9.50 .3740	0.90 .0354	0.15 .006	3.30 .130	7.20 .283	552	177	^		71,000	-
673	3.00		2.00	-	7.20	0.60	2.00	-	.3740	.0354			5.40	208	74		_	81,000	_
07.3	.1181	6.00 .2362	.0787	-	.2835	.0236	2.00 .0787	-	-	-	0.08 .003	3.60 .142	.213	200	/4	X	-	61,000	_
672/002	-							-	7.00	0.60		-	-	200	74	V V	_	80.000	
673/003	3.00 .1181	6.00 .2362	-	-	-	-	2.50 .0984	-	7.20 .2835	0.60 .0236	0.10 .004	3.60	5.40 .213	208	74	Х	10	80,000	KXX
600/60		7.00	3.00	3.80	-	-	.0984 3.00	3.80	.2833	.0230	0.10		.213 7.40	432	149	Х	v	80,000	50.000
683/63	3.00 .1181	.2751	.1181	3.80 .1496			.1181		-	-	.004	3.60 .142	.291	432	149	A	Х	80,000	50,000
683					0 10	0.50		.1496	0 10	0.90		-	-	432	149	v		90,000	53,000
000	3.00 .1181	7.00 .2756	2.00 .0787	2.80 .1102	8.10 .3189	0.50 .0197	3.00 .1181	3.80 .1496	8.10 .3189	0.80 .0315	0.10 .004	3.60	6.40 .252	432	149	X	XX	\$0,000	53,000
683/8	3.00		3.00	.1102 -	.3189		3.00		.3189	.0315			.232 7.40	432	149	X	X	95,000	55,000
003/0		8.00	.1181	-		-		3.80		-	0.10	3.60		432	149	^	~	93,000	55,000
	.1181	.3150	.1101				.1181	.1496			.004	.142	.291				201		

Note:

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GRW-		nensions in	Bearin	ng without clos	ure in [mm]	[inch]	Bear	ring with close	ure in [mm]	[inch]	Chamfer in		n dimensions		ngs acc. to	Closure v	variants ⁽³⁾	Max. limiting sp	eed ⁽⁵⁾ [mm ⁻¹]
designation		nm] nch]	Width without closure	Width with extended inner ring		imensions t closure	Width with extended inner ring	Width with extended inner ring	Flange d with c	imensions closure	[mm] [inch]	[n	DIN 5418 n m] nch]	DIN ISC) ⁽²⁾ (max)				
		1		without closure		1	with closure	with closure		1		Shaft diameter	Housing diameter		1		1		I
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
683/003	3.00	7.00	2.50	-	-	-	2.50	-	-	-	0.10	3.60	6.40	432	149	Х	-	93,000	-
	.1181	.2756	.0984				.0984				.004	.142	.252						
693/003	3.00	8.00	2.50	-	-	-	-	-	-	-	0.15	3.80	7.20	644	215	-	-	60,000	-
	.1181	.3150	.0984								.006	.150	.283						
693 (4)	3.00	8.00	3.00	3.80	9.50	0.70	4.00	4.80	9.50	0.90	0.15	3.80	7.20	644	215	Х	Х	80,000	51,000
	.1181	.3150	.1181	.1496	.3740	.0276	.1575	.1890	.3740	.0354	.006	.150	.283						
693/002	3.00	8.00	-	-	-	-	3.00	-	-	-	0.15	3.80	7.20	395	141	Х	-	67,000	-
11.	.1181	.3150					.1181				.006	.150	.283						
603	3.00	9.00	3.00	-	10.50	0.70	5.00	-	10.50	1.00	0.15	3.80	8.20	571	189	Х	-	67,000	-
	.1181	.3543	.1181		.4134	.0276	.1969		.4134	.0394	.006	.150	.323						
603/003	3.00	9.00	-	-	-	-	4.00	-	10.60	0.80	0.20	4.40	7.60	571	189	Х	-	67,000	-
	.1181	.3543					.1575		.4173	.0315	.008	.173	.299						
603/004	3.00	9.00	2.50	-	10.20	0.60	-	-	-	-	0.20	4.40	7.60	571	189	-	-	67,000	-
(00	.1181	.3543	.0984		.4016	.0236					.008	.173	.299	705	0.45		24	(5.000	11000
623	3.00 .1181	10.00 .3937	4.00 .1575	4.80 .1890	11.50 .4528	1.00 .0394	4.00 .1575	4.80 .1890	11.50 .4528	1.00 .0394	0.15 .006	4.40 .173	8.60 .339	725	265	Х	Х	65,000	44,000
623/13	3.00	.3937 13.00	4.00	4.80	.4320	.0394	4.00	4.80	.4320	.0394	0.15	4.40	.339 8.60	725	265	Х	Х	70,000	46,000
023/13	.1181	.5118	.1575	.1890	-	-	.1575	.1890	-	-	.006	.173	.339	725	203	~	^	70,000	40,000
633	3.00	13.00	5.00	-	15.00	1.00	5.00	.1070	15.00	1.00	0.20	4.80	11.20	1339	488	Х	_	55,000	
000	.1181	.5118	.1969		.5906	.0394	.1969		.5906	.0394	.008	.1890	.441	1007	400	Λ.		33,000	
693/0004	3.30	8.00	4.00	-	9.50	0.90	4.00	-	9.50	0.90	0.15	4.10	7.20	625	213	X	///_///	80,000	
07070004	.1299	.3150	.1575	_	.3740	.0354	.1575	_	.3740	.0354	.006	.161	.283	025	210			00,000	and the second second
674/004	4.00	7.00	1.60	-	-	-	1.60	_	-	-	0.08	4.50	6.50	337	129		_	60,000	_
0, 1, 001	.1575	.2756	.0630				.063				.003	.177	.256	0.07	127			00,000	
674	4.00	7.00	2.00	-	-	-	2.00	-	-	-	0.08	4.50	6.50	345	130	Х		67,000	
	.1575	.2756	.0787				.0787				.003	.177	.256						
674/003	4.00	7.00	2.50	-	-	-	2.50	-	8.20	0.60	0.08	4.50	6.50	255	108	Х	-	67,000	-
,	.1575	.2756	.0984				.0984		.3228	.0236	.003	.177	.256						
693B/0021	4.00	8.00	3.00	-	-	-	3.00	-	-	-	0.15	4.80	7.20	380	127	X		72,000	N N AV
	.1575	.3150	.1181				.1181				.006	.189	.283	IE			1	BENA	MAN
684	4.00	9.00	2.50	3.30	10.30	0.60	4.00	4.80	10.30	1.00	0.10	4.60	8.40	658	226	Х	Х	62,000	45,000
	.1575	.3543	.0984	.1299	.4055	.0236	.1575	.1890	.4055	.0394	.004	.181	.331						,
684/103	4.00	10.00	3.00	-	11.50	0.80	-	-	-	-	0.10	4.60	9.40	658	226	- /	ANT	48,000	_
	.1575	.3937	.1181		.4528	.0315					.004	.181	.370	NE C	1	KUIN	KILLA	De	
684/103	4.00	10.00	3.00	-	11.20	0.60	-	-	-	-	0.15	4.80	9.20	711	272	-	-	56,000	-
	.1575	.3937	.1181		.4409	.0236					.006	.189	.362						

Note:

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GRW- designation		nensions in	Bearir	ng without clos	ure in [mm]	[inch]	Bear	ring with close	ure in [mm]	[inch]	Chamfer in [mm]		n dimensions DIN 5418		ngs acc. to ⁽²⁾ (max)	Closure v	ariants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
designation	[ir	nm] nch]	Width without closure	Width with extended inner ring	Flange di without	imensions closure	Width with extended inner ring	Width with extended inner ring	Flange d with c	imensions closure	[inch]	[n	nm] nch]	Direiso	(indx)				
		1		without closure		I	with closure	with closure		1		Shaft diameter	Housing diameter		I		I		I
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} ⁽¹⁾	d _{a min}	D _{a max}	C, [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
684/10	4.00	10.00	4.00	4.80	11.50	1.00	4.00	4.80	11.50	1.00	0.10	4.60	9.40	711	272	Х	Х	86,000	45,000
	.1575	.3937	.1575	.1890	.4528	.0394	.1575	.1890	.4528	.0394	.004	.181	.370						
584/10 W8	4.00	10.00	-	-	-	-	4.00	-	11.60	0.80	0.15	4.80	9.20	711	272	Х	-	56,000	-
	.1575	.3937					.1575		.4567	.0315	.006	.189	.362						
594	4.00	11.00	4.00	-	12.50	1.00	4.00	-	12.50	1.00	0.15	4.80	10.20	730	271	Х	Х	66,000	41,000
	.1575	.4331	.1575		.4921	.0394	.1575		.4921	.0394	.006	.189	.402						
604	4.00	12.00	4.00	-	13.50	1.00	4.00	-	13.50	1.00	0.20	5.40	10.60	734	282	Х	Х	56,000	37,000
777 .	.1575	.4724	.1575		.5315	.0394	.1575		.5315	.0394	.008	.213	.417		(
524	4.00	13.00	5.00	5.80	15.00	1.00	5.00	5.80	15.00	1.00	0.20	5.80	11.20	1339	488	Х	Х	52,000	28,000
(04/100	.1575	.5118	.1969	.2283	.5906	.0394	.1969	.2283	.5906	.0394	.008	.228	.441	700	071	X	V	(5.000	50.000
594/133	4.00 .1575	13.00 .5118	5.00 .1969	-	-	-	5.00	-	-	-	0.15 .006	4.80 .189	12.20 .480	730	271	Х	Х	65,000	53,000
404/14	4.00	.5118 16.00	5.00	5.80	-	_	5.00	5.80	-	-	0.20	5.80	12.20	1306	486	Х	V	55,000	30,000
624/16	.1575	.6299	.1969	.2283	-	-	.1969	.2283	-	-	.008	.228	.480	1300	400	^	^	55,000	30,000
634	4.00	16.00	5.00	-	18.00	1.00	5.00	-	18.00	1.00	0.30	6.40	13.60	1730	670	X	Y	44,000	43,000
004	.1575	.6299	.1969		.7087	.0394	.1969		.7087	.0394	.012	.252	.535	17 50	0/0	~	~	44,000	40,000
624/17	4.00	17.00	5.00	5.80	-	-	5.00	5.80	-	-	0.20	5.80	15.20	1306	486	χ	Х	55,000	30,000
02.17.17	.1575	.6693	.1969	.2283			.1969	.2283			.008	.228	.598	1000	100			00,000	00,000
675	5.00	8.00	2.00	-	-	-	2.00	-	-	-	0.08	5.50	7.50	390	160	Х	-	52,000	_
	.1969	.3150	.0787				.0787				.003	.217	.295						
675/003	5.00	8.00	2.50	-	9.20	0.60	2.50	-	-	-	0.10	5.60	7.50	218	90	Х	///-///	63,000	
	.1969	.3150	.0984		.3622	.0236	.0984				.004	.220	.295					and the second second	7
675/004	5.00	8.00	3.00	-	-	-	3.00	-	-	-	0.08	5.40	7.60	390	160	Х	-	52,000	-
	.1969	.3150	.1181				.1181				.003	.213	.299						
675/094	5.00	9.00	3.00	-	-	-	3.00	-	10.20	0.60	0.15	5.40	8.60	431	169	Х	-	60,000	
	.1969	.3543	.1181				.1181		.4016	.0236	.006	.213	.339					and the	
694A/1002	5.00	10.00	4.00	-	-	-	4.00	-	11.20	0.80	0.15	5.50	8.80	431	169	Х	-	60,000	-
	.1969	.3937	.1575				.1575		.4409	.0315	.006	.217	.346						
594/1002	5.00	10.00	4.00	-	-	-	4.00	-	-	-	0.15	5.50	8.80	730	271	Х	-	66,000	XXXX
	.1969	.3937	.1575				.1575				.006	.217	.346				12	RXXX	NYA
594/1002 W1	5.00	10.00	4.00	-	11.60	0.80	4.00	-	11.60	0.80	0.15	5.80	9.20	431	169	Х	-	60,000	-
	.1969	.3937	.1575		.4567	.0315	.1575		.4567	.0315	.006	.228	.362						
585	5.00	11.00	3.00	-	12.50	0.80	5.00	-	12.50	1.00	0.15	5.80	10.70	734	282	X	XIE	71,000	37,000
	.1969	.4331	.1181		.4921	.0315	.1969		.4921	.0394	.006	.228	.421	M	1	AVID	RITH	July 1	
685/003	5.00	11.00	4.00	-	12.50	1.00	4.00	-	12.50	1.00	0.15	5.80	10.70	734	282	Х	-	62,000	-
	.1969	.4331	.1575		.4921	.0394	.1575		.4921	.0394	.006	.228	.421						

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability. • Subject to change due to technical improvement.





GRW- designation		mensions in nm]	Bearir	g without clos	ure in [mm]	[inch]	Bea	ring with close	ure in [mm]	[inch]	Chamfer in [mm]		n dimensions DIN 5418	Load ratin DIN ISO	igs acc. to	Closure v	variants ⁽³⁾	Max. limiting spe	ed ⁽⁵⁾ [mm ⁻¹]
designation	[ii	nch]	Width without closure	Width with extended inner ring	Flange d without	imensions closure	Width with extended inner ring	Width with extended inner ring	Flange di with c	imensions losure	[inch]	[n	nm] nch]	DIN 130	(indx)				
		1		without closure		L	with closure	with closure				Shaft diameter	Housing diameter		L				
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C, [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
695	5.00	13.00	4.00	-	15.00	1.00	4.00	-	15.00	1.00	0.20	6.40	11.60	1077	432	Х	Х	50,000	34,000
	.1969	.5118	.1575		.5906	.0394	.1575		.5906	.0394	.008	.252	.457						
624/0003	5.00	13.00	5.00	-	-	-	5.00	-	15.00	1.00	0.20	6.80	11.20	1306	486	Х	-	52,000	-
	.1969	.5118	.1969				.1969		.5906	.0394	.008	.268	.441	1000	507			50.000	
605	5.00	14.00	5.00	-	16.00	1.00	5.00	-	16.00	1.00	0.20	6.40	12.60	1329	507	Х	Х	50,000	33,000
105	.1969	.5512	.1969	5.00	.6299	.0394	.1969	5.00	.6299	.0394	.008	.252	.496	1700	675	V	V	50.000	21.000
625	5.00 .1969	16.00 .6299	5.00 .1969	5.80 .2283	18.00 .7087	1.00 .0394	5.00 .1969	5.80 .2283	18.00 .7087	1.00 .0394	0.30 .012	7.40 .291	13.60 .535	1729	0/5	Х	X	50,000	31,000
635	5.00	.0299 19.00	6.00	.2203	22.00	1.50	6.00	.2203	22.00	1.50	0.30	.291 7.40	.555 16.60	2522	1057	Х	X	40,000	22,000
033	.1969	.7480	.2362	-	.8661	.0591	.2362	-	.8661	.0591	.012	.291	.654	ZJZZ	1037	~	~	40,000	22,000
635/22	5.00	22.00	6.00	6.80	-	-	6.00	6.80	-	-	0.60	7.40	19.60	2458	1053	Х	X	43,000	25,000
000, 22	.1969	.8661	.2362	.2677			.2362	.2677			.024	.291	.772	2100	1000			,	20,000
676	6.00	10.00	2.50	-	11.20	0.60	-	-	-	-	0.15	6.80	9.20	500	216	_	_	35,000	_
	.2362	.3937	.0984		.4409	.0236					.006	.268	.362					,	
676/003	6.00	10.00	3.00	-	-	-	3.00	-	-	-	0.10	6.60	9.40	503	215	Х	-	46,000	-
	.2362	.3937	.1181				.1181				.004	.26	.370						
676/003	6.00	10.00	-	-	-	-	3.00	-	11.20	0.60	0.15	6.80	9.20	500	216	Х	-	35,000	-
	.2362	.3937					.1181		.4409	.0236	.006	.268	.362						111111
695/1232	6.00	12.00	3.00	-	13.20	0.60	-	-	-	-	0.20	7.40	10.60	716	295	-	-	50,000	-
	.2362	.4724	.1181		.5197	.0236					.008	.291	.417						
695/1202	6.00	12.00	4.00	-	13.60	0.80	4.00	-	13.60	0.80	0.15	6.80	11.20	851	366	X	X	49,000	28,000
	.2362	.4724	.1575		.5354	.0315	.1575		.5354	.0315	.006	.268	.441						
686	6.00	13.00	3.50	4.30	15.00	1.00	5.00	5.80	15.00	1.10	0.15	6.80	12.20	1096	437	Х	Х	55,000	33,000
	.2362	.5118	.1307	.1693	.5906	.0394	.1969	.2283	.5906	.0433	.006	.268	.48		- 1- 10				
696	6.00	15.00	5.00	-	17.00	1.20	5.00	-	17.00	1.20	0.20	7.40	13.60	1340	523	X	X	46,000	45,000
(05/0000	.2362	.5906	.1969		.6693	.0472	.1969		.6693	.0472	.008	.291	.535	1///	(1)	V		41.000	
625/0002	6.00 .2362	16.00 .6299	5.00 .1969	-	18.00 .7087	1.00 .0394	5.00 .1969	-	18.00 .7087	1.00 .0394	0.15 .006	8.40 .331	13.60 .535	1646	663	Х	-	41,000	-
606	-	-												2262	0.46	v v	X	15 000	20.000
606	6.00 .2362	17.00 .6693	6.00 .2362	-	19.00 .7480	1.20 .0472	6.00 .2362	-	19.00 .7480	1.20 .0472	0.30 .012	8.00 .315	15.00 .591	2263	846	Х	A 10	45,000	30,000
626	6.00	19.00	6.00	-	22.00	1.50	6.00	_	22.00	1.50	0.30	.313 8.40	.591 16.60	2522	1057	Х	X	40,000	22,000
020	.2362	.7480	.2362	_	.8661	.0591	.2362		.8661	.0591	.012	.331	.654	LJLL	1037	Λ	~	40,000	22,000
626/005	6.00	19.00	8.00	-	-	.0371	8.00	-	-	-	0.30	8.40	16.60	2522	1057	Х	41 N3	48,000	_
220,000	.2362	.7480	.3150				.3150				.012	.331	.654		1		SI MS	10,000	
636	6.00	22.00	7.00	-	-	-	7.00	-	-	-	0.30	8.40	19.60	3333	1423	X		36,000	-
	.2362	.8661	.2756				.2756				.012	.331	.772					,	

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW-		mensions in	Bearir	g without closu	ure in [mm]	[inch]	Bear	ring with closu	ure in [mm]	[inch]	Chamfer in		n dimensions		igs acc. to	Closure v	variants ⁽³⁾	Max. limiting spe	ed ⁽⁵⁾ [mm ⁻¹]
designation	[n [ii	nm] nch]	Width without closure	Width with extended inner ring	Flange di without	imensions closure	Width with extended inner ring	Width with extended inner ring	Flange di with c	imensions losure	[mm] [inch]	[n	DIN 5418 1 m] nch]	DIN ISO	⁽²⁾ (max)				
		1		without closure		L		with closure				Shaft diameter	Housing diameter		L		1		
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal (4)	with closure or with shield	with seal
677	7.00	11.00	2.50	-	12.20	0.60	-	-	-	-	0.10	7.60	10.40	461	206	-	-	50,000	_
	.2756	.4331	.0984		.4803	.0236					.004	.299	.409						
677/003	7.00	11.00	3.00	-	-	-	3.00	-	12.20	0.60	0.10	7.60	10.40	461	206	Х	-	50,000	-
	.2756	.4331	.1181				.1181		.4803	.0236	.004	.299	.409						
688A/1322	7.00	13.00	3.00	-	14.20	0.60	4.00	-	14.60	0.80	0.15	8.40	11.60	541	276	Х	Х	48,000	30,000
(00 (1000	.2756	.5118	.1181		.5591	.0236	.1575		.5748	.0315	.006	.331	.457	0.0.5	1.50	Х		25.000	
688/1322	7.00 .2756	13.00 .5118	-	-	-	-	4.00 .1575	-	-	-	0.20 .008	8.40 .331	11.60 .457	335	152	X	-	35,000	_
687	7.00	14.00	3.50	_	16.00	1.00	5.00	-	16.00	1.10	0.15	7.80	13.20	1186	505	Х	X	50,000	31,000
007	.2756	.5512	.1307	_	.6299	.0394	.1969	-	.6299	.0433	.006	.307	.520	1100	505	Λ	Λ	30,000	51,000
697	7.00	17.00	5.00	-	19.00	1.20	5.00	-	19.00	1.20	0.30	9.00	15.00	1795	776	Х	Х	39,000	28,000
0 //	.2756	.6693	.1969		.7480	.0472	.1969		.7480	.0472	.012	.354	.591	17 70	,,,,	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	07,000	20,000
607	7.00	19.00	6.00	-	22.00	1.50	6.00	-	22.00	1.50	0.30	9.00	17.00	3400	1057	Х	Х	43,000	22,000
	.2756	.7480	.2362		.8661	.0591	.2362		.8661	.0591	.012	.350	.669					,	,
627	7.00	22.00	7.00	-	25.00	1.50	7.00	-	25.00	1.50	0.30	9.40	19.60	3369	1363	Х	Х	35,000	21,000
	.2756	.8661	.2756		.9843	.0591	.2756		.9843	.0591	.012	.370	.772						
627/28	7.00	28.00	7.00	7.80	-	-	7.00	7.80	-	-	0.30	9.40	25.80	3369	1363	Х	-	40,000	_
	.2756	1.1024	.2756	.3071			.2756	.3071			.012	.370	1.016						1111
678	8.00	12.00	2.50	-	13.20	0.60	-	-	-	-	0.10	8.60	11.40	540	275	-	-	48,000	-
	.3150	.4724	.0984		.5197	.0236					.004	.339	.449						
678/003	8.00	12.00	-	-	-	-	3.50	-	13.60	0.80	0.10	8.60	11.40	540	275	X	<u></u>	48,000	
	.3150	.4724					.1307		.5354	.0315	.004	.339	.449			1.11		- And - Contraction	
688A/144	8.00	14.00	3.50	-	15.60	0.80	-	-	-	-	0.15	8.80	13.20	817	386	-	-	45,000	-
	.3150	.5512	.1307		.6142	.0315					.006	.346	.520						
688A/142	8.00	14.00	-	-	-	-	4.00	-	15.60	0.80	0.20	9.40	12.60	817	386	X	-	47,000	
	.3150	.5512					.1575		.6142	.0315	.008	.370	.496	1705				10.000	
688	8.00	16.00	4.00	-	18.00	1.00	6.00	-	18.00	1.30	0.20	9.40	14.60	1795	776	Х	Х	48,000	28,000
(00 (000	.3150	.6299	.1575		.7087	.0394	.2362		.7087	.0512	.008	.370	.575	1705	77/	F N		10.000	N N AV/
688/002	8.00	16.00	-	-	-	-	4.00	-	-	-	0.20	9.40	14.60	1795	776	Х		48,000	XXX
600/000	.3150	.6299	5.00		10.00	1.10	.1575		10.00	1.10	.008	.370	.575	1705	774	V	V	12 000	20.000
688/003	8.00 .3150	16.00 .6299	5.00 .1969	-	18.00 .7087	1.10 .0433	5.00 .1969	-	18.00 .7087	1.10 .0433	0.20 .008	9.40 .370	14.60 .575	1795	776	Х	Х	43,000	28,000
698	.3150 8.00	.0299 19.00	6.00	-	22.00	.0433 1.50	6.00	-	22.00	.0433 1.50	0.30	10.00	.575 17.00	2240	917	Х	AX NO	43,000	27,000
070	.3150	.7480	.2362	-	.8661	.0591	.2362	-	.8661	.0591	.012	.394	.669	2240		^	SHA DE	40,000	27,000
688/20	8.00	20.00	4.00	4.80	-	.0391	.2302	-	-	-	0.20	9.40	18.60	1795	776	- AYID	-	45,000	_
000/20	.3150	.7874	.1575	.1890							.008	.370	.732	1775	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			-0,000	

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW- designation		nensions in nm]	Bearir	ng without clos	ure in [mm]	[inch]	Bear	ring with close	ure in [mm]	[inch]	Chamfer in [mm]		n dimensions DIN 5418		ngs acc. to ⁽²⁾ (max)	Closure v	ariants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
designation	[in	nch]	Width without closure	Width with extended inner ring		imensions closure	Width with extended inner ring	Width with extended inner ring	Flange di with c	imensions closure	[inch]	[n	nm] nch]	Dirvise	(inux)				
		1		without closure		I		with closure				Shaft diameter	Housing diameter		I				
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
608/003	8.00	22.00	6.00	-	-	-	-	-	-	-	0.30	10.00	20.00	3369	1363	-	_	38,000	-
	.3150	.8661	.2362								.012	.394	.787						
608	8.00	22.00	7.00	-	25.00	1.50	7.00	-	25.00	1.50	0.30	10.00	20.00	3369	1363	Х	Х	38,000	21,000
	.3150	.8661	.2756		.9843	.0591	.2756		.9843	.0591	.012	.394	.787						
608/005	8.00	22.00	10.00	-	-	-	10.00	-	-	-	0.30	10.00	20.00	3369	1363	Х	-	43,000	-
	.3150	.8661	.3937				.3937				.012	.394	.787						
608/006	8.00	22.00	10.31	-	-	-	10.31	-	-	-	0.30	10.00	20.00	3369	1363	Х	Х	43,000	29,000
608/007	.3150	.8661	.4059				.4059				.012	.394	.787	22/0	10/0	X	V	42,000	00.000
008/00/	8.00 .3150	22.00 .8661	11.00 .4331	-	-	-	11.00 .4331	-	-	-	0.30 .012	10.00 .394	20.00 .787	3369	1363	Å	A	43,000	29,000
628	8.00	24.00	8.00	-	_	_	8.00	-	-	-	0.30	10.40	21.60	3360	1430	X	Y	38,000	21,000
520	.3150	.9449	.3150	_	_	-	.3150	_	-	-	.012	.409	.850	5500	1450	Λ	Λ.	30,000	21,000
6000/0001	8.00	26.00	8.00	-	-	-	8.00	-	-	-	0.30	10.40	24.00	4698	1982	X	_	35,000	_
0000/0001	.3150	1.0236	.3150				.3150				.012	.409	.945	1070	1702			00,000	
638	8.00	28.00	9.00	-	-	-	9.00	-	-	-	0.30	10.40	25.60	4563	1982	Х	-	34,000	_
	.3150	1.1024	.3543				.3543				.012	.409	1.008					,	
679	9.00	14.00	3.00	-	15.50	0.80	-	-	-	-	0.10	9.60	13.40	919	468	-	_	42,000	_
	.3543	.5512	.1181		.6102	.0315					.004	.378	.528						
679/003	9.00	14.00	4.50	-	15.50	0.80	4.50	-	15.50	0.80	0.10	9.60	13.40	919	468	Х	Х	42,000	25,000
	.3543	.5512	.1772		.6102	.0315	.1772		.6102	.0315	.004	.378	.528						
689	9.00	17.00	4.00	4.80	19.00	1.00	6.00	-	19.00	1.30	0.20	10.40	15.60	1798	797	X	Х	44,000	27,000
	.3543	.6693	.1575	.1890	.7480	.0394	.2362		.7480	.0512	.008	.409	.614			1.11	<u> </u>	AND PROPERTY AND	7
689/003	9.00	17.00	5.00	-	-	-	5.00	-	-	-	0.20	10.40	15.60	1798	797	Х	-	44,000	-
	.3543	.6693	.1969				.1969				.008	.409	.614						
699	9.00	20.00	6.00	6.80	23.00	1.50	6.00	6.80	23.00	1.50	0.30	11.00	18.00	2467	1081	X	X	40,000	25,000
	.3543	.7874	.2362	.2677	.9055	.0591	.2362	.2677	.9055	.0591	.012	.433	.709		1420				
609	9.00	24.00	7.00	-	27.00	1.50	7.00	-	27.00	1.50	0.30	11.00	22.00	3435	1430	Х	Х	33,000	20,000
	.3543	.9449	.2756		1.0630	.0591	.2756		1.0630	.0591	.012	.433	.866	1100	1000	7			N No byo
629	9.00	26.00	8.00	8.80	28.00	2.00	8.00	8.80	28.00	2.00	0.30	11.40	23.60	4698	1982	Х	X	34,000	19,000
4700	.3543	1.0236	.3150	.3465	1.1024	.0787	.3150	.3465	1.1024	.0787	.012	.449	.929	055	405		Nan Jeje	17.000	ANA
6700	10.00 .3937	15.00	3.00	-	16.50	0.80	-	-	16.50	0.80	0.15	10.80	1 4.20	855	435	-	-	17,000	-
6700/003		.5906	.1181		.6496	.0315	4.00		.6496	.0315	.006	.425	.559	855	435	V	CAX NO	17,000	10,000
0/00/003	10.00 .3937	15.00 .5906	4.00 .1575	-	16.50 .6496	0.80 .0315	4.00 .1575	-	16.50 .6496	0.80 .0315	0.15 .006	10.80 .425	1 4.20 .559	000	433	X	2402	17,000	10,000
6800 (4)	.3937 10.00	.5908 19.00	5.00	5.80	.0490 21.00	1.00	7.00	7.80	.0490 21.00	1.50	0.30	.425 12.00	.559 17.00	1922	915	X	X	42,000	25,000
0000	.3937	.7480	.1969	.2283	.8268	.0394	.2756	.3071	.8268	.0591	.012	.472	.669	1722	715	Λ	Λ	42,000	23,000

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW-		mensions in	Bearir	ng without clos	ure in [mm]	[inch]	Bea	ring with close	ure in [mm]	[inch]	Chamfer in		n dimensions	Load ratir	ngs acc. to	Closure v	ariants ⁽³⁾	Max. limiting sp	eed ⁽⁵⁾ [mm ⁻¹]
designation	L n [ir	nm] nch]	Width without closure	Width with extended inner ring		imensions closure	Width with extended inner ring	Width with extended inner ring	Flange d with c	imensions closure	[mm] [inch]	[n	DIN 5418 nm] nch]	DIN ISC) ^[2] (max)				
		1	closure	without closure		1		with closure		1		Shaft diameter	Housing diameter		1				I
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	(1) r _{s min}	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
6800/002	10.00	19.00	-	-	-	-	5.00	-	21.00	1.00	0.30	12.00	17.00	1922	915	Х	_	34,000	-
	.3937	.7480					.1969		.8268	.0394	.012	.472	.669						
6800/003	10.00	19.00	6.00	-	-	-	6.00	-	-	-	0.30	12.00	17.00	1922	915	Х	-	35,000	-
	.3937	.7480	.2362				.2362				.012	.472	.669						
6800/202	10.00	20.00	-	-	-	-	5.00	-	-	-	0.30	12.00	18.00	1922	915	Х	-	34,000	-
	.3937	.7874					.1969				.012	.472	.709						
6900	10.00	22.00	6.00	-	25.00	1.50	6.00	-	25.00	1.50	0.30	12.00	20.00	2695	1273	Х	Х	41,000	24,000
1000	.3937	.8661	.2362		.9843	.0591	.2362		.9843	.0591	.012	.472	.787		1000				10.000
6000	10.00	26.00	8.00	8.80	28.00	2.00	8.00	8.80	28.00	2.00	0.30	12.40	23.60	4698	1982	Х	Х	35,000	19,000
(000 (000	.3937	1.0236	.3150	.3465	1.1024	.0787	.3150	.3465	1.1024	.0787	.012	.488	.929	(1) (0)	1000	X		00.000	
6000/003	10.00 .3937	26.00 1.0236	10.00 .3937	-	-	-	10.00 .3937	-	-	-	0.30 .012	12.40 .488	23.60 .929	4149	1388	Х	-	38,000	-
16100	.3937 10.00	28.00	.393/ 8.00	-	-	_	.3937 8.00	_	-	-	0.30	.488 14.20	.929 23.80	4620	1960	X		37,000	_
16100	.3937	1.1024	.3150	-	-	-	.3150	-	-	-	.012	.559	23.60 .937	4020	1900	^	_	37,000	_
6200	10.00	30.00	9.00	-	-	-	9.00	-	-	-	0.60	14.20	25.80	4340	1920	X	Y	27,000	18,000
0200	.3937	1.1811	.3543				.3543				.024	.559	1.016	4340	1720	~	~	27,000	10,000
6300	10.00	35.00	11.00	-	-	-	11.00	-	-	-	0.60	14.20	20.80	6870	2750	X	X	27,000	18,000
	.3937	1.3780	.4331				.4331				.024	.559	.819	00,0	2,00			27,000	
6701	12.00	18.00	4.00	-	19.50	0.80	4.00	-	19.50	0.80	0.20	13.40	16.60	926	530	Х	Х	15,000	10,000
	.4724	.7087	.1575		.7677	.0315	.1575		.7677	.0315	.008	.528	.654						
6801	12.00	21.00	5.00	-	-	-	5.00	-	-	-	0.30	14.00	19.00	1930	900	Х	///-///	30,000	
	.4724	.8268	.1969				.1969				.012	.551	.748					and the second second	7
6801/003	12.00	21.00	6.00	-	-	-	6.00	-	-	-	0.30	14.00	19.00	1720	840	Х	-	32,000	-
	.4724	.8268	.2362				.2362				.012	.551	.748						
6801/004	12.00	21.00	7.00	-	23.00	1.50	7.00	-	23.00	1.50	0.30	14.00	19.00	1915	1041	Х	X	39000	24,000
	.4724	.8268	.2756		.9055	.0591	.2756		.9055	.0591	.012	.551	.748					the state	
6901	12.00	24.00	6.00	-	-	-	6.00	-	-	-	0.30	14.00	22.00	2971	1460	Х	-	32,000	-
	.4724	.9449	.2362				.2362				.012	.551	.866						
16001	12.00	28.00	7.00	-	-	-	7.00	-	-	-	0.30	14.00	26.00	5100	2370	-	-	32,000	
	.4724	1.1024	.2756				.2756				.012	.551	1.024				1 de	RXXX	MMM
6001	12.00	28.00	8.00	-	30.00	2.00	8.00	-	30.00	2.00	0.30	14.00	26.00	5237	2370	Х	Х	31,000	17,000
	.4724	1.1024	.3150		1.1811	.0787	.3150		1.1811	.0787	.012	.551	1.024						
6001/003	12.00	28.00	11.00	-	-	-	11.00	-	-	-	0.30	14.00	26.00	5237	2359	Х	ALA	31,000	-
	.4724	1.1024	.4331				.4331				.012	.551	1.024	Me de la companya de	1	KID	KILLAR	Dr.	
63001	12.00	28.00	12.00	-	-	-	12.00	-	-	-	0.50	14.00	26.00	5100	2370	Х	Х	30,000	16,000
	.4724	1.1024	.4724				.4724				.020	.551	1.024						

Note:

⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius.
⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer.
⁽³⁾ Different shields or seals available.
⁽⁴⁾ Bearings also available with 1 or 2 shields/seals.

⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW- designation		mensions in	Bearir	ng without clos	ure in [mm]	[inch]	Bea	ring with clos	ure in [mm]	[inch]	Chamfer in [mm]		on dimensions DIN 5418		ngs acc. to ⁽²⁾ (max)	Closure	variants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
designation	[n [ii	nm] nch]	Width without closure	Width with extended inner ring		imensions closure	Width with extended inner ring	Width with extended inner ring	Flange di with c	imensions closure	[mm] [inch]	[n	n m] nch]	Dirvise	(max)				
		1		without closure		1		with closure				Shaft diameter	Housing diameter		L		1		
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
16101	12.00	30.00	8.00	-	-	-	8.00	-	-	-	0.50	14.40	27.60	5070	2360	Х	Х	28,000	16,000
	.4724	1.1811	.3150				.3150				.020	.567	1.087						
6201	12.00	32.00	10.00	-	-	-	10.00	-	-	-	0.60	16.20	27.80	5770	2450	Х	Х	26,000	15,000
	.4724	1.2598	.3937				.3937				.024	.638	1.094						
62201	12.00	32.00	14.00	-	-	-	14.00	-	-	-	0.60	16.20	27.80	6890	3100	Х	Х	25,000	15,000
	.4724	1.2598	.5512				.5512				.024	.638	1.094						
6301	12.00	37.00	12.00	-	-	-	12.00	-	-	-	1.00	17.60	31.40	8240	3360	Х	Х	25,000	14,000
(2001	.4724	1.4567	.4724				.4724				.039	.693	1.236	00.10	00/0		N	07.000	14.000
62301	12.00	37.00	17.00	-	-	-	17.00	-	-	-	1.00	17.60	31.40	8240	3360	-	Х	27,000	14,000
(700	.4724	1.4567	.6693				.6693				.039	.693	1.236	937	582	V	V	12,000	9000
6702	15.00 .5906	21.00 .8268	4.00 .1575	-	-	-	4.00 .1575	-	-	-	0.20 .008	16.40 .646	19.60 .772	937	382	Х	Å	13,000	9000
6802	15.00	24.00	5.00	-	-	-	5.00	-	-	-	0.30	17.00	22.00	2080	1100	Х	Y	25,000	15,000
0002	.5906	.9449	.1969	-	_	_	.1969	_	-	-	.012	.669	.866	2000	1100	~	~	23,000	13,000
6802/003	15.00	24.00	7.00	-	26.00	1.50	7.00	-	26.00	1.50	0.30	17.00	22.00	2073	1253	Х	Х	33,000	18,000
0002/000	.5906	.9449	.2756	_	1.0236	.0591	.2756	_	1.0236	.0591	.012	.669	.866	2070	1200	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	00,000	10,000
6902	15.00	28.00	7.00	-	-	-	7.00	-	-	-	0.30	17.00	26.00	4445	2268	Х	Х	24,000	16,000
	.5906	1.1024	.2756				.2756				.012	.669	1.024						
16002	15.00	32.00	8.00	-	-	-	8.00	-	-	-	0.50	17.00	30.00	5600	2830	Х	Х	26,000	14,000
	.5906	1.2598	.3150				.3150				.020	.669	1.181						
6002	15.00	32.00	9.00	-	-	-	9.00	-	-	-	0.30	17.00	30.00	5676	2819	X	///-///	25,000	
	.5906	1.2598	.3543				.3543				.012	.669	1.181					and the second second	7
6202	15.00	35.00	11.00	-	-	-	11.00	-	-	-	0.60	19.20	30.80	6490	3000	Х	Х	24,000	16,000
	.5906	1.3780	.4331				.4331				.024	.756	1.213						
62202	15.00	35.00	14.00	-	-	-	14.00	-	-	-	0.60	19.20	30.80	7650	3750	Х	X	23,000	13,000
	.5906	1.3780	.5512				.5512				.024	.756	1.213		112				
6302	15.00	42.00	13.00	-	-	-	13.00	-	-	-	1.50	24.00	33.00	11400	5450	Х	Х	21,000	11,000
	.5906	1.6535	.5118				.5118				.059	.945	1.299						
6703	17.00	23.00	4.00	-	24.50	0.80	4.00	-	24.50	0.80	0.20	18.40	21.60	1000	658	Х	X	11,000	7,000
	.6693	.9055	.1575		.9646	.0315	.1575		.9646	.0315	.008	.724	.850				JE.	KNX	NYM
6803	17.00	26.00	5.00	-	-	-	5.00	-	-	-	0.30	19.00	24.00	2240	1270	Х	-	22,000	-
	.6693	1.0236	.1969				.1969				.012	.748	.945	N. France	- 14			34.54	
6903	17.00	30.00	7.00	-	-	-	7.00	-	-	-	0.30	19.00	28.00	4723	2547	X	HAN	21,000	_
	.6693	1.1811	.2756				.2756				.012	.748	1.102	M	10	AND	XHIX	J.	
16003	17.00	35.00	8.00	-	-	-	8.00	-	-	-	0.30	19.00	33.00	6000	3250	Х	-	23,500	-
	.6693	1.378	.3150				.3150				.012	.748	1.299						

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW- designation		mensions in	Bearir	ng without clos	ure in [mm]	[inch]	Bea	ring with clos	ure in [mm]	[inch]	Chamfer in [mm]		n dimensions DIN 5418		ngs acc. to) ⁽²⁾ (max)	Closure v	ariants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
designation	[ii	nm] nch]	Width without closure	Width with extended inner ring	Flange d without	imensions closure	Width with extended inner ring	Width with extended inner ring		imensions closure	[inch]	[n	1m] nch]	DIN ISC	(max)				
		1		without closure		I		with closure		1		Shaft diameter	Housing diameter		1				
Basic symbols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} ⁽¹⁾	d _{a min}	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
6003	17.00	35.00	10.00	-	-	-	10.00	-	-	-	0.30	19.00	33.00	5090	2630	Х	Х	23,000	18,000
	.6693	1.3780	.3937				.3937				.012	.748	1.299						
6203	17.00	40.00	12.00	-	-	-	12.00	-	-	-	0.60	21.20	35.80	8130	3850	Х	Х	20,000	15,000
	.6693	1.5748	.4724				.4724				.024	.835	1.409						
62203	17.00	40.00	16.00	-	-	-	16.00	-	-	-	0.60	21.20	35.80	9560	4750	Х	-	21,000	-
	.6693	1.5748	.6299				.6299				.024	.835	1.409						
6303	17.00	47.00	14.00	-	-	-	14.00	-	-	-	1.00	22.60	41.40	11550	5330	Х	Х	18,000	14,000
170.1	.6693	1.8504	.5512				.5512				.039	.890	1.630	2,400	700			10.000	7.000
6704	20.00	27.00	4.00	-	28.50	0.80	4.00	-	28.50	0.80	0.20	5.40	25.60	1402	729	Х	Х	10,000	7,000
6804	.7874	1.0630	.1575		1.122	.0315	.1575		1.122	.0315	.008	.213	1.008	4015	2462	X	V	25,000	12,000
0804	20.00 .7874	32.00 1.2598	7.00 .2756	-	35.00 1.378	1.50 .0591	7.00 .2756	-	35.00 1.378	1.50 .0591	0.30 .012	22.00 .866	30.00 1.181	4015	2402	Å	A	25,000	13,000
6904	20.00	37.00	9.00	-	40.00	2.00	9.00	2.00	40.00	2.00	0.30	22.00	35.00	6381	3682	X	Y	23,000	12,000
0904	.7874	1.4567	.3543	-	1.5748	.0787	.3543	.0787	1.5748	.0787	.012	.866	1.378	0301	3002	~	~	23,000	12,000
16004	20.00	42.00	8.00	-	-	.07 07	8.00	.07 07	-	.07 07	0.30	22.00	40.00	6940	4100	X	_	21,000	_
10001	.7874	1.6535	.3150				.3150				.012	.866	1.575	0710	1100			21,000	
6004	20.00	42.00	12.00	-	-	-	12.00	-	-	-	1.00	24.60	37.40	7900	4250	Х	Х	21,000	11,000
	.7874	1.6535	.4724				.4724				.039	.969	1.472						
6204	20.00	47.00	14.00	-	-	-	14.00	-	-	-	1.00	25.60	41.40	10910	5360	Х	Х	17,000	10,000
	.7874	1.8504	.5512				.5512				.039	1.008	1.630					, i	, i i i i i i i i i i i i i i i i i i i
6705	25.00	32.00	4.00	-	-	-	4.00	-	34.00	1.00	0.20	5.40	30.60	1091	838	- /	X	12,000	8,000
	.9843	1.2598	.1575				.1575		1.3386	.0394	.008	.213	1.205					A DESCRIPTION OF THE OWNER OWNER OF THE OWNER OWNER OF THE OWNER OWNE	7
6805	25.00	37.00	7.00	-	40.00	1.50	7.00	-	40.00	1.50	0.30	27.00	35.00	4303	2932	Х	-	21,000	-
	.9843	1.4567	.2756		1.5748	.0591	.2756		1.5748	.0591	.012	1.063	1.378						
6905	25.00	42.00	9.00	-	45.00	2.00	9.00	-	45.00	2.00	0.30	27.00	40.00	7001	4540	Х	X	19,000	10,000
	.9843	1.6535	.3543		1.7717	.0787	.3543		1.7717	.0787	.012	1.063	1.575		11/2			Line Child	
16005	25.00	47.00	8.00	-	-	-	8.00	-	-	-	0.60	27.00	45.00	8550	4690	Х	-	17,000	-
	.9843	1.8504	.3150				.3150				.024	1.063	1.772						N/ XX/ XX //
6005	25.00	47.00	12.00	-	-	-	12.00	-	-	-	0.60	28.20	43.80	8550	4690	Х	X	18,000	9,500
	.9843	1.8504	.4724				.4724				.024	1.110	1.724				Je je	AN N K	YXXX
6706	30.00	37.00	4.00	-	39.00	1.00	4.00	-	39.00	1.00	0.20	5.40	35.60	1143	947	Х	-	17,000	-
1001	1.1811	1.4567	.1575		1.5354	.0394	.1575		1.5354	.0394	.008	.213	1.402	N. Karala	Al				
6806	30.00	42.00	7.00	-	45.00	1.50	7.00	-	45.00	1.50	0.30	32.00	40.00	4538	3402	X	XIS	18,000	9,000
1001	1.1811	1.6535	.2756		1.7717	.0591	.2756		1.7717	.0591	.012	1.260	1.575	70.10	5000	AND	XHHX	17.000	0.505
6906	30.00	47.00	9.00	-	50.00	2.00	9.00	-	50.00	2.00	0.30	32.00	45.00	7242	5003	Х	Х	17,000	8,500
	1.1811	1.8504	.3543		1.9685	.0787	.3543		1.9685	.0787	.012	1.260	1.772				20V		

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

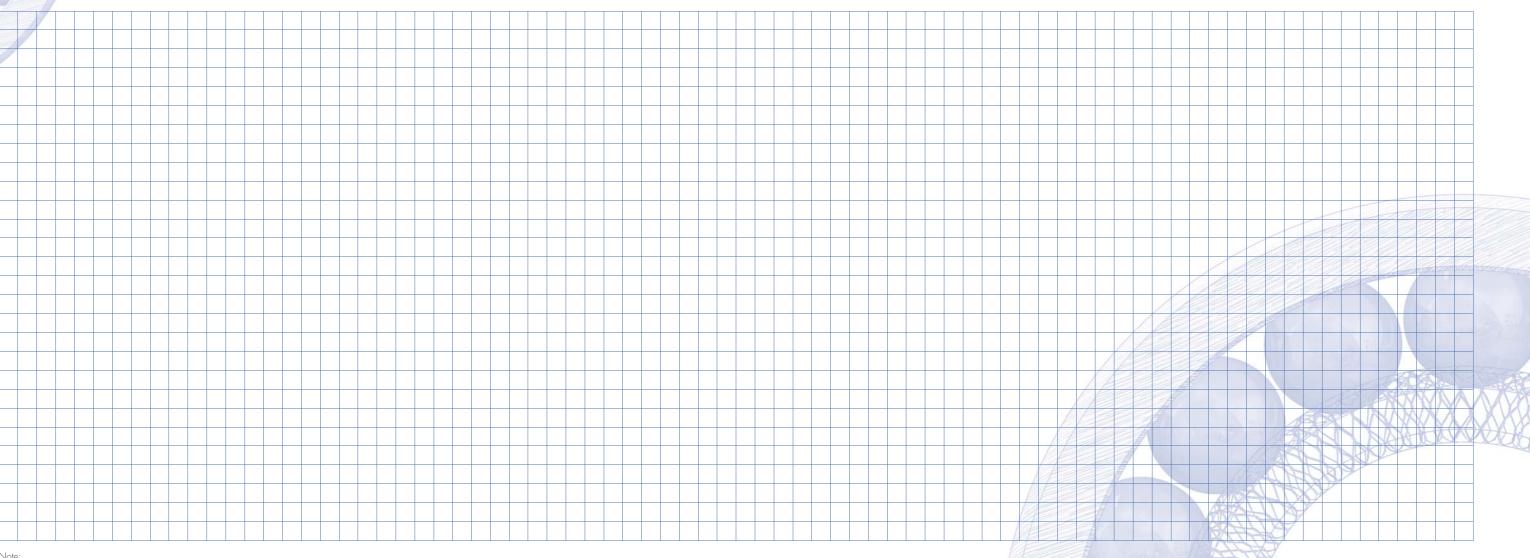
availability. • Subject to change due to technical improvement.





GRW- designatio	n	Main dim [m [ind		Bearin Width without closure	ng without clos Width with extended inner ring without closure		imensions closure	Width with extended	Width with extended inner ring	with cl	mensions	Chamfer in [mm] [inch]	acc. to D	n dimensions NN 5418 m] ch] Housing diameter	Load ratin DIN ISO	•	Closure v	ariants ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
Basic syml	bols	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} ⁽¹⁾	$d_{\alpha \min}$	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	with closure or with shield	with seal
6807		35.00	47.00	7.00	-	50.00	1.50	7.00	-	50.00	1.50	0.30	37.00	45.00	4729	3821	Х	Х	16,000	8,000
		1.3780	1.8504	.2756		1.9685	.0591	.2756		1.9685	.0591	.012	1.457	1.772						

Your Notes



Note:

⁽¹⁾ $r_{s \min}$ = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non-standard retainer. ⁽³⁾ Different shields or seals available.

^[4] Bearings also available with 1 or 2 shields/seals.

⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW designation	[m	nensions in nm]	Bearir Wldth	ng without clos Width with	1	[inch] nensions wit-	Bea Width with	ring with clos Width with		i nch] imensions	Chamfer in [mm]	to ANSI/AFE	dimensions acc. 3MA Std. 12.2 in		ngs acc. to ⁽²⁾ (max)	Closure	variants ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
	lin	ch]	without	extended		closure	closure	extended	with c	closure	[inch]		[mm] i nch]						
			closure	inner ring without closure				inner ring with closure				Shaft diameter	Housing diameter						
Basic symobls	d	D	В	B1	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C [Ń]	C _{or} [N]	Shield ⁽⁴⁾	Packing ⁽⁴⁾	with closure or with shield	shield
1016	1.016	3.175	1.191	-	-	-	-	-	-	-	0.08	1.50	2.65	106	28	-	-	150,000	-
	.0400	.1250	.0469								.003	.059	.104						
1191	1.191	3.967	1.588	2.381	5.156	0.330	-	-	-	-	0.08	1.80	3.35	163	44	-	-	129,000	-
	.0469	.1562	.0625	.0937	.2030	.0130					.003	.071	.132						
1397	1.397	4.763	1.984	-	-	-	2.779	-	5.944	0.787	0.08	2.00	4.15	239	67	Х	-	114,000	-
	.0550	.1875	.0781				.1094		.2340	.03100	.003	.079	.163						
5/64	1.984	6.350	2.380	3.175	7.518	0.584	3.571	4.366	7.518	0.787	0.08	2.60	5.75	286	90	Х	-	95000	-
2017	.0781	.2500	.0937	.1250	.2960	.0230	.1406	.1719	.2960	.0310	.003	.102	.226						
2380	2.380	4.763	1.588	2.380	5.944	0.457	2.380	3.175	5.944	0.787	0.08	2.90	4.25	192	59	Х	—	94,000	-
	.0937	.1875	.0625	.0937	.2340	.0180	.0937	.1250	.2340	.0310	.003	.114	.167						
3175/0002	2.380	6.350	2.779	-	7.518	0.787	2.779	-	7.518	0.787	0.08	2.95	5.75	292	97	Х	-	82,000	-
. (0.0	.0937	.2500	.1094	0.571	.2960	.0310	.1094	1.0//	.2960	.0310	.003	.116	.226		015	N N	N	(0.000	51.000
3/32	2.380	7.938	2.779	3.571	9.119	0.584	3.571	4.366	9.119	0.787	0.08	3.10	7.25	644	215	Х	Х	62,000	51,000
0175/000	.0937	.3125	.1094	.1406	.3590	.0230	.1406	.1719	.3590	.0310	.003	.122	.285	011	100	V		00.000	
3175/002	3.175	6.350	-	-	-	-	2.380 .0937	-	7.518 .2960	0.584	0.08	3.75 .148	5.75 .226	311	109	Х	-	80,000	-
3175	.1250	.2500 6.350	2.380	3.175	7.518	0.584		3.571		.0230 0.787	.003	3.75		292	97	Х	X	80.000	52,000
31/3	3.175						2.779 .1094		7.518		0.08		5.75	292	97	Å	~	80,000	53,000
3175A	.1250 3.175	.2500 6.350	.0937 2.380	.1250	.2960 7.518	.0230 0.584	2.779	.1406	.2960 7.518	.0310 0.787	.003 0.08	.148 3.75	.226 5.75	311	109	Х	_	80,000	
317 JA	.1 250	.2500	.0937	_	.316 .2960	.0230	.1094	_	.316 .2960	.0310	.003	.148	.226	311	104	^	_	80,000	_
1/8A	3.175	7.938	2.779	3.571	9.119	0.584	3.571	4.366	9.119	0.787	0.08	3.90	7.20	644	215	X	V	65,000	51,000
17 OA	.1250	.3125	.1094	.1406	.3590	.0230	.1406	4.300 .1719	.3590	.0310	.003	.154	.283	044	215	^	^	03,000	51,000
3175/061	3.175	9.525	2.779	_	.5570	.0230	2.779	.1717		_	0.08	3.90	8.80	292	97	X	_	80,000	_
517 57 001	.1250	.3750	.1094				.1094				.003	.154	.346	272	77	Λ		00,000	
3175/6	3.175	9.525	-	-	_	_	2.779	_	_	-	0.08	3.90	8.80	292	97	χ		80,000	
017070	.1250	.3750					.1094				.003	.154	.346					00,000	
1/8A/6	3.175	9.525	_	_	_	_	3.571	4.366	10.719	0.787	0.08	3.90	8.80	644	215	Х	Х	82,000	51,000
17 07 0	.1250	.3750					.1406	.1719	.4220	.0310	.003	.154	.346	011	210	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		02,000	01,000
1/8B	3.175	9.525	3.967	4.763	11.176	0.762	3.967	4.763	11.176	0.762	0.30	4.55	8.25	720	260	Х	X	61,000	44,000
, ==	.1250	.3750	.1562	.1875	.4400	.0300	.1562	.1875	.4400	.0300	.012	.179	.325	The			12	BENN	
3175/552	3.175	10.414	_	-	-	-	2.380	-	_	-	0.08	3.75	8.40	292	97	Х	-	80,000	<u>-</u>
,	.1250	.4100					.0937				.003	.148	.331					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
3175/8	3.175	12.700	_	-	_	_	2.779	3.571	_	-	0.08	4.55	11.35	292	97	X	ANT	80,000	_
	.1250	.5000					.1094	.1406			.003	.179	.447			- Ann	ALIAN	St.	
1/8B/083	3.175	12.700	4.366	-	-	-	4.366	-	-	-	0.30	4.55	11.35	725	265	X	-	74,000	-
, . ,	.1250	.5000	.1719				.1719				.012	.179	.447					/	

Note:

Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non standard retainer ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW designation		nensions in nm]	Beari	ng without clos	ure in [mm] [[inch]	Bea	ring with clos	ure in [mm] [i	inch]	Chamfer in [mm]		dimensions acc. MA Std. 12.2 in		ngs acc. to) ⁽²⁾ (max)	Closure v	variants ⁽³⁾	Max. limiting sp	eed ⁽⁵⁾ [mm ⁻¹]
dosignation	[in	ich]	Wldth without closure	Width with extended inner ring		ensions wit- closure	Width with closure	Width with extended inner ring		imensions closure	[inch]	[r	nm] nch]	5	(max)				
		1		without closure		1		with closure		1		Shaft diameter	Housing diameter		1		L		L
Basic symobls	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} ⁽¹⁾	$d_{\alpha \ min}$	D _{a max}	C [Ń]	C _{0r} [N]	Shield ⁽⁴⁾	Packing ⁽⁴⁾	with closure or with shield	shield
3967/002	3.967	7.938	-	-	-	-	2.779	-	-	-	0.08	4.55	7.30	391	165	Х	-	65,000	_
	.1562	.3125					.1094				.003	.179	.287						
3967	3.967	7.938	2.779	3.571	9.119	0.584	3.175	3.967	9.119	0.914	0.08	4.55	7.30	391	165	Х	Х	68,000	42,000
	.1562	.3125	.1094	.1406	.3590	.0230	.1250	.1562	.3590	.0360	.003	.179	.287						
4763A/002	4.763	7.938	-	-	-	-	2.779	-	-	-	0.08	5.35	7.30	391	165	Х	-	61,000	-
	.1875	.3125					.1094				.003	.211	.287						
4763A	4.763	7.938	2.779	3.571	9.119	0.584	3.175	3.967	9.119	0.914	0.08	5.35	7.30	391	165	Х	Х	65,000	42,000
- 119	.1875	.3125	.1094	.1406	.3590	.0230	.1250	.1562	.3590	.0360	.003	.211	.287						
4763A/062	4.763	9.525	2.779	-	-	-	2.779	-	-	-	0.08	5.35	7.30	391	165	Х	Х	65,000	42,000
	.1875	.3750	.1094				.1094				.003	.211	.287						
4763B	4.763	9.525	3.175	3.967	10.719	0.584	3.175	3.967	10.719	0.787	0.08	5.50	8.80	730	271	Х	Х	56,000	41,000
	.1875	.3750	.1250	.1562	.4220	.0230	.1250	.1562	.4220	.0310	.003	.217	.346						
4763A/082	4.763	12.700	-	-	-	-	2.779	3.571	-	-	0.08	5.35	8.80	391	165	Х	-	70,000	-
	.1875	.5000					.1094	.1406			.003	.211	.346						
4763B/083	4.763	12.700	3.967	-	-	-	3.967	-	-	-	0.08	6.20	11.35	730	271	Х	-	56,000	-
0 (1) (1000	.1875	.5000	.1562				.1562				.003	.244	.447	1000	100			50.000	
3/16/002	4.763	12.700	-	-	-	-	3.967	-	-	-	0.30	6.20	11.35	1339	488	Х	-	50,000	
0 /1 /	.1875	.5000	0.0/7	1710	14.051	1.0/7	.1562	c 77 1	14051	1.0/7	.012	.244	.447	1000	100	24	N/	50,000	07.000
3/16	4.763	12.700	3.967	4.763	14.351	1.067	4.978	5.771	14.351	1.067	0.30	6.20	11.35	1339	488	Х	Х	50,000	37,000
47/00/004	.1875	.5000	.1562	.1875	.5000	.0420	.1960	.2272	.5000	.0420	.012	.244	.447	700	071			10,000	
4763B/084	4.763 .1875	12.700	2.779 .1094	-	-	-	5.558	-	-	-	0.30	6.20 .244	11.35 .447	730	271	-//		43,000	
1/4A/0001	4.763	.5000	4.978		17.526	1.067	.2188 4.978		17.526	1.067	.012 0.30	.244 6.20		1651	670	V	v	41,000	21.000
1/4A/0001	4.703 .1875	.6250	4.978 .1960	_	.6900	.0420	4.978 .196	_	.6900	.0420	.012	0.20 .244	14.35 .565	1031	070	A	A	41,000	31,000
62501	6.350			3.967	10.719	0.584	3.175	3.967	10.719	0.914		6.90	8.95	391	165	V	V	54,000	35,000
6350A	.2500	9.525 .3750	3.175 .1250	.1562	.4220	.02300	.1250	.1562	.4220	.0360	0.08 .003	.272	.352	271	105	A	~	54,000	33,000
6350B	6.350	12.700	3.175	3.967	13.894	0.584	4.763	5.558	13.894	1.143	0.13	7.20	11.85	730	271	Х	Х	38,000	33000
00000	.2500	.5000	.1250	.1562	.5000	.02300	.1875	.2188	.5000	.0450	.005	.283	.467	/ 50	2/1	Λ	~	50,000	33000
1/4A	6.350	15.875	4.978	5.771	17.526	1.067	4.978	5.771	17.526	1.067	0.30	7.85	14.35	1651	670	Х	X	43,000	31,000
1/4/	.2500	.6250	4.97 0 .1960	.2272	.6900	.0420	4.97 0 .1960	.2272	.6900	.0420	.012	.309	.565	1051	0/0	Λ		40,000	51,000
1/4/002	6.350	19.050	-	_	_	-	5.558	-	_	-	0.41	8.20	17.20	2522	1057	Х	X	35,000	28,000
17 47 002	.2500	.7500					.2188				.016	.323	.677	LJLL	1007	Λ	~	00,000	20,000
1/4	6.350	19.050	5.558	_	_	_	7.142	_	_	-	0.41	8.20	17.20	2522	1057	X	XX	35,000	28,000
• / •	.2500	.7500	.2188				.2812				.016	.323	.677	L'UL	1		AM DE	20,000	20,000
7938	7.938	12.700	3.967	4.763	13.894	0.787	3.967	4.763	13.894	0.787	0.13	8.80	11.85	539	279	X	X	45,000	30,000
	.3125	.5000	.1562	.1875	.5000	.03100	.1562	.1875	.5000	.0310	.005	.346	.467	007	277	~	~	10,000	00,000
	.3123	.3000	.1302	.10/5	.3000	.03100	.1302	.10/5	.5000	.0310	.005			·					

Note:

⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius.
⁽²⁾ Other load ratings are possible due to different ball sets with use of a non standard retainer
⁽³⁾ Different shields or seals available.
⁽⁴⁾ Bearings also available with 1 or 2 shields/seals.

⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.

availability.

• Subject to change due to technical improvement.





GRW		nensions in	Beari	ng without clos	oure in [mm] [inch]	Bea	ring with clos	ure in [mm] [i	nch]	Chamfer in		limensions acc.		igs acc. to	Closure v	ariants ⁽³⁾	Max. limiting sp	eed ⁽⁵⁾ [mm ⁻¹]
designation	[n [in	nm] I ch]	Wldth without closure	extended inner ring	Flange dim hout c	ensions wit- losure	Width with closure	extended inner ring	Flange di with c		[mm] [inch]	[m	AA Std. 12.2 in m] ch]	DIN ISO	⁽²⁾ (max)				
				without closure				with closure				Shaft diameter	Housing diameter						
Basic symobls	d	D	В	B1	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C [Ń]	C _{0r} [N]	Shield ⁽⁴⁾	Packing ⁽⁴⁾	with closure or with shield	shield
9525	9.525	15.875	3.967	-	-	-	3.967	-	-	-	0.25	11.05	14.35	856	435	Х	-	35,000	—
	.3750	.6250	.1562				.1562				.010	.435	.565						
3/8/002	9.525	22.225	-	-	-	-	5.558	-	-	-	0.41	11.45	20.30	2555	1129	Х	-	30,000	-
	.3750	.8750					.2188				.016	.451	.799						
3/8	9.525	22.225	5.558	-	24.613	1.575	7.142	-	24.613	1.575	0.41	11.45	20.30	2555	1129	Х	Х	30,000	24,000
	.3750	.8750	.2188		.9690	.0620	.2812		.9690	.0620	.016	.451	.799						
12700A/002	12.700	19.050	-	-	-	-	3.967	-	-	-	0.25	14.20	17.55	918	542	Х	Х	28,000	20,000
	.5000	.7500					.1562				.010	.500	.691						
12700B	12.700	22.225	7.142	-	-	-	7.142	-	-	-	0.41	14.20	20.30	1972	1144	Х	-	28,000	-
	.5000	.8750	.2812				.2812				.016	.500	.799						
1/2	12.700	28.575	6.350	-	31.115	1.575	7.938	-	31.115	1.575	0.41	15.90	26.05	5108	2413	Х	Х	32,000	21,000
	.5000	1.1250	.2500		1.2250	.0620	.3125		1.2250	.0620	.016	.626	1.026						
15875A	15.875	22.225	3.967	-	-	-	3.967	-	-	-	0.25	19.05	20.30	1133	801	Х	-	25,000	-
	.6250	.8750	.1562				.1562				.010	.750	.799						
5/8	15.875	34.925	7.142	-	-	-	8.733	-	37.846	1.745	0.80	19.05	31.75	5999	3265	Х	-	25,000	-
	.6250	1.3750	.2812				.3438		1.4900	.0687	.031	.750	1.250						

Note:

- Note: ⁽¹⁾ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius. ⁽²⁾ Other load ratings are possible due to different ball sets with use of a non standard retainer ⁽³⁾ Different shields or seals available. ⁽⁴⁾ Bearings also available with 1 or 2 shields/seals. ⁽⁵⁾ Limiting speed also depends on seal material and the respective ball set.



• Subject to change due to technical improvement.





Spindle / angular contact bearings

Spindle bearings are single-row angular contact bearings with a nominal contact angle of 15° (C) or 25° (E). They can be subjected to both radial and (in one direction) axial loads. The direction of the axial load carrying capacity is shown by a "V" marking on the outer ring. GRW spindle ball bearings are suitable for applications requiring precision while carrying high loads combined with high speeds.

GRW spindle ball bearings are characterised by the following properties:

- Manufactured quality of P4 (or ABEC7) or better.
- Rings generally made of corrosion-resistant SV 30 high-grade steel.
- Steel or ceramic balls.
- Solid retainer made from fiber-reinforced phenolic resin or special materials, for applications involving higher temperatures.
- 15° (C) or 25° (E) contact angles are standard.
- Optionally, bearings can be paired and ground to three pre-defined preload classes (L, M, S) or to a specific customer defined preload.
- Oil or grease lubrication.
- Open and shielded versions available.
- Cleanroom assembly, lubrication and packaging.



Open spindle ball bearings

- Standard configuration has large balls for optimum utilisation of bearing geometries and a solid retainer for higher bearing capacities.
- The outer ring has only one partial shoulder remaining. This partial shoulder is necessary to prevent the , bearing from separation.
- Solid outer ring guided retainer with a low profile cross-section is particularly well suited for oil injection lubrication.

Shielded spindle ball bearings

- Non-contact shields do not add any additional torque caused by the shields.
- Standard shields made of Viton (VZ) coupled with a stainless steel support shield offer excellent temperature and debris resistance.
- A very small, closely toleranced sealing gap provides protection against dust particles.
- GRW recommends using a grease lubricant for longer life and reliability.
- Dimensionally identical to non-shielded spindle bearings.
- This type of design often requires use of smaller balls that results in a lower load capacity but higher axial stiffness and speed limits (usually signified by an 'A', 'B', ... after the base type).
- Also available without shields for high-speed applications.

Handling

- GRW recommends to keep the bearing in its airtight packaging until it is ready for assembly.
- Extreme cleanliness during assembly is recommended.
- Avoid dropping or subjecting the bearing to any kind of impact loading.
- Spindle bearings are designed to handle axial loads in only one direction. This direction is identified by the "V" laser marking on the outer ring.
- Using the proper assembly tooling will prevent damage to the bearing.
- Duplex bearings labeled (DB), (DF), or (DT) are always packed in pairs and can only be used as pairs in the specified configuration.
- Universally matched Duplex bearings can be used in every combination of configurations, i.e. you can combine bearings from different packages or lots. These bearings may be assembled in any duplex arrangement.
- Prior to running bearings at high speed a run in period helps to distribute lubricant and is beneficial for the bearing!

Duplex bearings

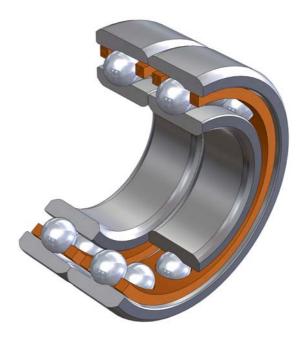
Duplex bearings are two matched bearings that provide the following performance benefits:

- Accurate bearing alignment in radial and axial directions including defined clearances and controlled stiffness.
- Increased system reliability.
- Higher load capacities.

Duplexing of these bearings is performed by loading each bearing with the specified preload and accurately grinding the inner and/or outer rings until the bearing faces of both rings are flush.

Paired bearings machined this way are designed to be assembled in the following configurations: back-to-back (DB), face-to-face (DF) or tandem (DT) and axially loaded to the specified or required force. Duplexed bearings are designed to provide the specified preload when the ground surfaces are accurately pressed together.

The ball bearings must be mounted according to the designation on the packaging labels or "V" markings on the outer rings.





Deep groove radial bearings:

For deep groove Duplex bearings the radial play is bigger than normal to facilitate the desired contact angle, rigidity and axial load capacity.

Unless otherwise specified, GRW grind duplex deep groove radial bearings to a preload of 5 N and a nominal contact angle of 15°. If necessary, preload and contact angles can be adjusted to a customer's unique operating requirements.

Spindle ball bearings:

Preload and the contact angle are generally standardised for spindle bearings. GRW's standard contact angles are 15° (C) or 25° (E), preloads are specified as light (L), medium (M) or strong (S). If necessary, preloads and contact angles can be customised to each customer's individual operating reauirements.

	By default, GRW uses for	:
	Deep groove radial bearings	Spindle bea- rings
Contact angle α	15° (C)	15° (C) or 25° (E)
Preload FV	5 N	L, M, S

However, the preload should not be specified higher than necessary as this would result in an increase of start up and running torque, which in turn would directly affect the expected life of the bearina.

To achieve an identical fit for both bearings, Duplex bearings are sorted into two groups. The bore and outer diameters are packaged in pairs with bearings from the same group. To take full advantage of these duplexed pairs, they should also be mounted with calibrated shafts and housings (see the chapter "Grading of bore and outside diameters"). Bearing fits should be carefully selected because an interference fit on the inner or outer ring will change the preload.



Installation and configuration of duplexed bearings

O (<>) arrangement: Back to back (designation -1 and DB for spindle bearings)

With this bearing configuration the inner rings are designed to be clamped together. The contact angle load path between the outer ring raceway, the ball and the inner ring curvature diverge, which results in maximum stability and stiffness against any moment loading. Radial and axial loads can be taken in both directions.

X (><) arrangement: Face to face (designation -2 and DF for spindle bearings)

With this bearing configuration, the inner rings are designed to be clamped together. The load path converges resulting in less stability and a lower stiffness against moment loading. This design more easily compensates any misalignment of the assembly. Radial and axial loads can likewise be taken in both directions.

Tandem (>>) or (<<) arrangement (designation -3 and DT for spindle bearings)

Duplex bearings in O- and X- configurations are designed to accommodate axial loading in both directions. The tandem-mounted bearing design is capable of taking a significantly higher axial load, but only in one direction. With this type of bearing, preloading and control of axial play can only be achieved by preloading against another bearing.

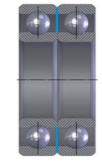
General: Bearings of these pairing types are packed in pairs or sets and must not be mixed

Universal Tandem arrangement (designation -4 and DT for spindle bearings).

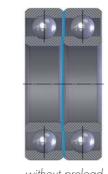
Universally matched bearing pairs have a significant advantage compared to the duplexed designs described above. They are individually ground in such a way that they can be assembled in various pairing configurations, e.g. X, O, or tandem; without any loss in performance. With the same preload, these single bearings can be interchanged without any problems.



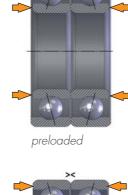
without preload



without preload

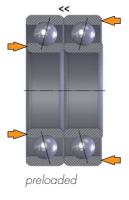


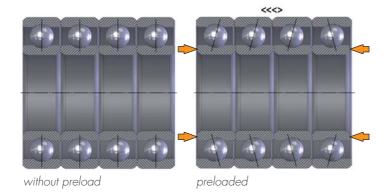
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preloaded





Bearing sets

When a higher stiffness is specified, multiple duplexed bearing configurations may be used together to get the desired results. Depending on the application, these bearing sets can be made up of universally

Usual designation	Mark/ arrangement	Permissible load direction	Rigidity
O -arrangement -1 or DB	\Leftrightarrow	axial radial	axial radial rigidity against tilting torques
X -arrangement -2 or DF	><	axial radial	axial radial
Tandem arrangement −3 or DT	<< or >>	radial and unilate- rally axial	unilaterally radial
Universal −4 or U	<<>< Examples: >< or <> or >> or	axial radial	depending on the arrangement
Set of bearings assem- bled from universally matched bearings	><< Examples: <>>		depending on the arrangement

Superduplex bearings

Superduplex bearings are double-row deep groove radial bearings or angular contact bearings where either the inner or outer rings are integral and the remaining rings are separate to allow assembly and correct preloading. (See also chapter "Special bearings" \rightarrow Superduplex bearings or Extraduplex bearings).

For Superduplex bearings, the following configurations apply:



paired bearings in X, O, or tandem configurations. The table below shows some examples of possible configurations in more detail.

- designation -5
 O-configuration (<>)
 (corresponds to designation -1)
- designation –6 X-configuration (><) (corresponds to designation –2)
- designation –7
 Tandem (corresponds to designation –3)



Designation system of spindle ball bearings





									0	
	TA TB AC2TA		- X XB		- U DB		- L M	- %		- L G
	L2TA		XD X4 X4B X4D		DF DT		s /X			L299
TA TB	solid retainer made of fiber-reinforced phenolic resin guided by outer ring same as TA, guided by inner ring	- X XB	without diameter grading bore and outside diameter graded in 2 classes bore graded in	- U Bea	single bearing not duplexed universally duplexed ring pair:	- L M S	without preload light medium heavy/ strong	 Standard grease quantitiy 20 % of free bearing volume with closed spindle bearing adjusted lubricant 	-	open bearing are preserved with oil LOO1 closed bearings are greased with 20% grease
т×А -та -тв	other retainer materials available on request angular contact shoulder on outer ring (standard)	XD X4	2 classes outside diameter graded in 2 classes bore and outside diameter graded in 4 classes	DF	2 bearings in O-arrangement 2 bearings in X-arrangement 2 bearings in	/х	preload value in [N] if other than L, M, S.	quantity in [%] of free bearing volume	L	G510 as a standard Oil Grease
AC2	angular contact shoulder on inner ring (standard)	X4B	in 4 classes bore graded in 4 classes	DT	2 bearings in Tandem arrangement	Exam	ple:		L299	dry bearing
l2ta	inner ring can be dismounted, solid retainer keeps the balls	X4D	outside diameter graded in 4 classes			Spino U/10	le ball bearing) (= universally d with 10 N			





Spindle ball bearings

GRW designation	Mo	ain dimension [mm] [inch]	ns in	Load r acc. to [I	Ball set	Limiting s	peeds*		Preloa	d
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) nedium [N]	(S) heav [N]
C bearings, open, n	netric											
SV723 C TA	3.00	10.00 .3937	4.00 .1575	170	506	8	1.588 .0625	254,000	209,000	5	8]
HYSV723 C TA	3.00 .1181	10.00 .3937	4.00 .1575	119	506	8	1.588 .0625	373,000	269,000	5	8	
SV774 C TA	4.00 .1575	7.00 .2756	2.00 .0787	77	223	10	1.000 .0394	309,000	255,000	5	7	
HYSV774 C TA	4.00 .1 <i>5</i> 75	7.00 .2756	2.00 .0787	54	223	10	1.000 .0394	455,000	327,000	5	7	
SV724 C TA	4.00 .1575	13.00 .5118	5.00 .1969	364	1037	8	2.381 .0937	195,000	161,000	5	16	
HYSV724 C TA	4.00 .1575	13.00 .5118	5.00 .1969	255	1037	8	2.381 .0937	287,000	206,000	5	16	
SV734 C TA	4.00 .1575	16.00 .6299	5.00 .1969	721	1594	9	2.500 .0984	1 <i>57</i> ,000	130,000	8	24	
HYSV734 C TA	4.00 .1575	16.00 .6299	5.00 .1969	504	1594	9	2.500 .0984	231,000	167,000	8	24	
SV725 C TA	5.00 .1969	16.00 .6299	5.00 .1969	721	1594	9	2.500 .0984	1 <i>57</i> ,000	130,000	8	24	
HYSV725 C TA	5.00 .1969	16.00 .6299	5.00 .1969	504	1594	9	2.500 .0984	231,000	167,000	8	24	
SV735 C TA	5.00 .1969	19.00 .7480	6.00 .2362	1277	2612	10	3.175 .1250	127,000	105,000	13	40	
HYSV735 C TA	5.00 .1969	19.00 .7480	6.00 .2362	894	2612	10	3.175 .1250	187,000	135,000	13	40	
SV786 C TA	6.00 .2362	13.00 .5118	3.50 .1378	354	895	10	1.984 .0781	175,000	144,000	5	14	
HYSV786 C TA	6.00 .2362	13 .5118	3.50 .1378	247	895	10	1.984 .0781	258,000	186,000	5	14	
SV786 E TA	6.00 .2362	13.00 .5118	3.50 .1378	332	856	10	1.984 .0781	149,000	123,000	5	14	
HYSV786 E TA	6.00 .2362	13.00 .5118	3.50 .1378	232	856	10	1.984 .0781	219,000		5	14	
SV786/001 C TA HYSV786/001 C TA	6.00 .2362 6.00	13.00 .5118 13.00	5.00 .1969 5.00	354 247	895 895	10	1.984 .0781 1.984	175,000	144,000	5	14	
SV726 C TA	.2362 6.00	.5118 19.00	.1969 6.00	1277	2612	10	.0781 3.175	127,000	105,000	13	40	
HYSV726 C TA	.2362 6.00	.7480 19.00	.2362 6.00	894	2612	10	.1250 3.175	187,000	135,000	13	40	
SV707 C TA	.2362 7.00	.7480 19.00	.2362 6.00	1277	2612	10	.1250 3.175	127,000	105,000	13	40	
HYSV707 C TA	.2756 7.00	.7480 19.00	.2362 6.00	894	2612	10	.1250 3.175	187,000	135,000	13	40	
SV727 C TA	.2756 7.00	.7480 22.00	.2362 7.00	1693	3511	9	.1250 3.969	116,000	95,000	18	54	1
HYSV727 C TA	.2756	.8661 22.00	.2756 7.00	1185	3511	9	.1563 3.969	170,000	122,000	18	54	1
SV788 C TA	.2756 8.00	.8661 16.00	.2756 4.00	569	1377	10	.1563 2.500	142,000	117,000	7	21	
	.3150	.6299	.1575			-	.0984	,	,			

GRW designation	Mo	iin dimensior [mm] [inch]	ns in	Load r acc. to [Ball set	Limiting s	peeds*		Preload	
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light n [N]	(M) nedium [N]	(S) heavy [N]
C bearings, open, m	etric											
HYSV788 C TA	8.00 .3150	16.00 .6299	4.00 .1575	398	1377	10	2.500 .0984	208,000	150,000	7	21	42
SV788 E TA	8.00	16.00	4.00	534	1317	10	2.500	120,000	99,000	7	21	42
	.3150	.6299	.1575				.0984					
HYSV788 E TA	8.00	16.00	4.00	374	1317	10	2.500	177,000	128,000	7	21	4
	.3150	.6299	.1575	1/00	0.511	0	.0984	11/ 000	05.000	10	5.4	10
SV708 C TA	8.00 .3150	22.00 .8661	7.00 .2756	1693	3511	9	3.969 .1563	116,000	95,000	18	54	10
HYSV708 C TA	.3130 8.00	22.00	7.00	1185	3511	9	3.969	170,000	122,000	18	54	10
THSV/00C IA	.3150	.8661	.2756	1105	5511	7	.1563	170,000	122,000	10	54	10
SV708 E TA	8.00	22.00	7.00	1589	3358	9	3.969	98,000	81,000	18	54	10
077 00 E 171	.3150	.8661	.2756	1007	0000		.1563	,0,000	01,000	10	0-	10
HYSV708 E TA	8.00	22.00	7.00	1112	3358	9	3.969	145,000	104,000	18	54	10
	.3150	.8661	.2756				.1563		. ,			
SV789 C TA	9.00	17.00	4.00	642	1471	11	2.500	131,000	108,000	8	23	4
	.3543	.6693	.1575				.0984					
HYSV789 C TA	9.00	17.00	4.00	450	1471	11	2.500	192,000	138,000	8	23	4
	.3543	.6693	.1575				.0984					
SV709 C TA	9.00	24.00	7.00	1974	3844	10	3.969	105,000	86,000	20	59	11
	.3543	.9449	.2756				.1563					
HYSV709 C TA	9.00	24.00	7.00	1382	3844	10	3.969	154,000	111,000	20	59	11
	.3543	.9449	.2756	0707	5107	1.0	.1563	0.4.000	70.000		70	
SV729 C TA	9.00	26.00	8.00	2737	5137	10	4.763	94,000	78,000	26	79	15
	.3543	1.0236	.3150	1017	C107	10	.1875	120,000	10,000	01	70	15
HYSV729 C TA	9.00 .3543	26.00 1.0236	8.00 .3150	1916	5137	10	4.763 .1875	139,000	10,000	26	79	I D
SV7800 C TA	.5545 10.00	19.00	5.00	724	1556	12	2.500	117,000	97,000	8	24	4
577000 C 1A	.3937	.7480	.1969	/ 24	1550	ΙZ	.0984	117,000	97,000	0	24	4
HYSV7800 C TA	10.00	19.00	5.00	507	1556	12	2.500	172,000	124,000	8	24	4
11100/0000 C 1/(.3937	.7480	.1969	00/	1000	12	.0984	172,000	124,000	0	2-7	
SV7800 E TA	10.00	19.00	5.00	680	1488	12	2.500	10,0000	82,000	8	24	4
	.3937	.7480	.1969		16		.0984					
HYSV7800 E TA	10.00	19.00	5.00	476	1488	12	2.500	147,000	106,000	8	24	4
	.3937	.7480	.1969				.0984					
SV7900 C TA	10.00	22.00	6.00	1500	2824	11	3.175	107,000	88,000	15	44	8
	.3937	.8661	.2362			đ	.1250		Nº 6	AXXX	XX	
HYSV7900 C TA	10.00	22.00	6.00	1050	2824	11	3.175	157,000	113,000	15	44	8
	.3937	.8661	.2362				.1250					
SV7900A E TA	10.00	22.00	6.00	1407	2700	11	3.175	90,000	74,000	15	44	8
	.3937	.8661	.2362		0705	1.2	.1250	100.000				-
HYSV7900A E TA	10.00	22.00	6.00	985	2700	11	3.175	133,000	96,000	15	44	8
	.3937	.8661	.2362	0707	E107	10	.1250	04,000	70.000	04	70	1.7
SV7000 C TA	10.00	26.00	8.00	2737	5137	10	4.763	94,000	78,000	26	79	15
HYSV7000 C TA	.3937	1.0236	.3150	1016	5107	10	.1875	139,000	10.000	26	79	15
H1377000 C 1A	10.00 .3937	26.00 1.0236	8.00 .3150	1916	5137	10	4.763 .1875	139,000	10,000	20	19	15

* The indicated speed limits are guide values for spring-loaded single bearings with low load; depending on the respective application, higher or lower speed limits may apply in practice.
** For use with oil lubrication, these bearings are also available without shields. Subject to change due to technical improvement.





Spindle ball bearings

GRW designation	Main dimensions in [mm] [inch]			Load ratings acc. to DIN ISO		Ball set		Limiting speeds*		Preload		
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) nedium [N]	(S) heav [N]
C bearings, open, m	netric											
SV7000 E TA	10.00	26.00	8.00	2568	4913	10	4.763	80,000	66,000	26	79	1.
HYSV7000 E TA	.3937 10.00	1.0236 26.00	.3150 8.00	1798	4913	10	.1875 4.763	118,000	85,000	26	79].
	.3937	1.0236	.3150	0.100			.1875					
SV7200 C TA	10.00 .3937	30.00 1.1811	9.00 .3543	3192	5597	11	4.763 .1875	83,000	68,000	29	86	1
HYSV7200 C TA	10.00	30.00	9.00	2235	5597	11	4.763	122,000	88,000	29	86	1
SV7200 E TA	.3937 10.00	1.1811 30.00	.3543 9.00	2995	5353	11	.1875 4.763	71,000	58,000	29	86	1
317 200 L IA	.3937	1.1811	.3543	2775	5555	11	.1875	71,000	50,000	27	00	
HYSV7200 E TA	10.00 .3937	30.00 1.1811	9.00 .3543	2097	5353	11	4.763 .1875	104,000	75,000	29	86	1
SV7801 C TA	12.00	21.00	5.00	794	1543	14	2.381	103,000	84,000	8	24	
	.4724	.8268	.1969				.0937					
HYSV7801 C TA	12.00 .4724	21.00 .8268	5.00 .1969	556	1543	14	2.381 .0937	151,000	109,000	8	24	
SV7801 E TA	12.00	21.00	5.00	745	1476	14	2.381	87,000	72,000	8	24	
	.4724	.8268	.1969	501	1 47/	1.4	.0937	100.000	00.000	0	0.4	
HYSV7801 E TA	12.00 .4724	21.00 .8268	5.00 .1969	521	1476	14	2.381 .0937	128,000	92,000	8	24	
SV7901 C TA	12.00	24.00	6.00	1700	2992	12	3.175	94,000	78,000	15	46	
HYSV7901 C TA	.4724 12.00	.9449 24.00	.2362 6.00	1190	2992	12	.1250 3.175	139,000	10,000	15	46	
1113V7 901 C 1A	.4724	.9449	.2362	1190	2992	ΙZ	.1250	137,000	10,000	15	40	
SV7901 E TA	12.00	24.00	6.00	1595	2861	12	3.175	80,000	66,000	15	46	
HYSV7901 E TA	.4724 12.00	.9449 24.00	.2362 6.00	1117	2861	12	.1250 3.175	118,000	85,000	15	46	
	.4724	.9449	.2362				.1250	,				
SV7001 C TA	12.00 .4724	28.00 1.1024	8.00 .3150	2590	4423	12	3.969 .1563	82,000	68,000	23	68	1
HYSV7001 C TA	.4/24 12.00	28.00	8.00	1813	4423	12	3.969	121,000	87,000	23	68	1
	.4724	1.1024	.3150				.1563					
SV7001 E TA	12.00 .4724	28.00 1.1024	8.00 .3150	2430	4230	12	3.969 .1563	70,000	58,000	23	68	1
HYSV7001 E TA	12.00	28.00	8.00	1701	4230	12	3.969	103,000	74,000	23	68	1
	.4724	1.1024	.3150	0.000/	74.50	0	.1563	77.000	(1 0 0 0		110	
SV7201C C TA	12.00 .4724	32.00 1.2598	10.00 .3937	3806	7652	9	5.953 .2344	77,000	64,000	39	118	2
HYSV7201C C TA	12.00	32.00	10.00	2664	7652	9	5.953	114,000	82,000	39	118	2
SV7201C E TA	.4724	1.2598	.3937	2571	7210	9	.2344	66.000	54.000	20	110	2
SV/ZUICE IA	12.00 .4724	32.00 1.2598	10.00 .3937	3571	7318	Ŷ	5.953 .2344	66,000	54,000	39	118	4
HYSV7201C E TA	12.00	32.00	10.00	2500	7318	9	5.953	97,000	70,000	39	118	2
SV7802 C TA	.4724 15.00	1.2598 24.00	.3937 5.00	1054	1784	18	.2344 2.381	87,000	72,000	9	27	
377 002 C IA	.5906	.9449	.1969	1004	., 04	10	.0937	07,000	, 2,000		2/	
HYSV7802 C TA	15.00 .5906	24.00 .9449	5.00 .1969	738	1784	18	2.381 .0937	128,000	92,000	9	27	
SV7802 E TA	15.00	.9449 24.00	5.00	989	1706	18	.0937 2.381	74,000	61,000	9	27	
	.5906	.9449	.1969			-	.0937	,	,			

GRW designation Basic symbols	Main dimensions in [mm] [inch]			Load ratings acc. to DIN ISO		Ball set		Limiting speeds*		Preload		
	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) medium [N]	(S) heavy [N]
C bearings, open, m	etric											
HYSV7802 E TA	15.00 .5906	24.00 .9449	5.00 .1969	692	1706	18	2.381 .0937	109,000	78,000	9	27	5
SV7902 C TA	15.00 .5906	28.00 1.1024	7.00 .2756	2841	4666	13	3.969 .1563	79,000	65,000	24	72	14
HYSV7902 C TA	15.00 .5906	28.00 1.1024	7.00 .2756	1989	4666	13	3.969	116,000	84,000	24	72	14
SV7902 E TA	15.00 .5906	28.00	7.00	2665	4463	13	3.969	67,000	55,000	24	72	14
HYSV7902 E TA	15.00	1.1024 28.00	.2756 7.00	1866	4463	13	.1563 3.969	99,000	71,000	24	72]2
SV7002 C TA	.5906 15.00	1.1024 32.00	.2756 9.00	3970	6327	13	.1563 4.763	72,000	60,000	32	97	19
HYSV7002 C TA	.5906 15.00	1.2598 32.00	.3543 9.00	2779	6327	13	.1875 4.763	106,000	77,000	32	97	19
SV7002 E TA	.5906 15.00	1.2598 32.00	.3543 9.00	3725	6051	13	.1875 4.763	62,000	51,000	32	97	19
HYSV7002 E TA	.5906 15.00	1.2598 32.00	.3543 9.00	2607	6051	13	.1875 4.763	90,000	65,000	32	97	19
sv7202 c ta	.5906 15.00	1.2598 35.00	.3543 11.00	4090	6970	13	.1875 4.763	97,000	63,000	30	60	12
SV7202 E TA	.5906	1.3780 35.00	.4331 11.00	3930	6650	13	.1875 4.763	85,000	55,000	45	90	18
	.5906	1.3780	.4331				.1875					
SV7803 C TA	17.00 .6693	26.00 1.0236	5.00 .1969	1071	1754	18	2.381 .0937	79,000	65,000	9	27	
HYSV7803 C TA	17.00 .6693	26.00 1.0236	5.00 .1969	750	1754	18	2.381 .0937	116,000	84,000	9	27	
SV7803 E TA	17.00 .6693	26.00 1.0236	5.00 .1969	1005	1677	18	2.381 .0937	67,000	55,000	9	27	
HYSV7803 E TA	17.00 .6693	26.00 1.0236	5.00 .1969	704	1677	18	2.381 .0937	99,000	71,000	9	27	
SV7903 C TA	17.00 .6693	30.00 1.1811	7.00 .2756	3137	4888	14	3.969 .1563	72,000	6,0000	25	75	13
HYSV7903 C TA	17.00 .6693	30.00	7.00 .2756	2196	4888	14	3.969 .1563	106,000	77,000	25	75	1.5
SV7903 E TA	17.00 .6693	30.00 1.1811	7.00 .2756	2944	4675	14	3.969 .1563	61,000	51,000	25	75	1:
HYSV7903 E TA	17.00 .6693	30.00 1.1811	7.00 .2756	2061	4675	14	3.969 .1563	90,000	65,000	25	75	13
SV7003 C TA	17.00	35.00	10.00 .3937	4571	6817	14	4.763	65,000	54,000	34	102	-20
HYSV7003 C TA	.6693 17.00	1.3780 35.00	10.00	3200	6817	14	.1875 4.763	96,000	69,000	34	102	20
SV7003 E TA	.6693 17.00	1.3780 35.00	.3937 10.00	4571	6817	14	.1875 4.763	56,000	46,000	34	102	20
HYSV7003 E TA	.6693 17.00	1.3780 35.00	.3937 10.00	3200	6817	14	.1875 4.763 .1875	82,000	59,000	34	102	20

* The indicated speed limits are guide values for spring-loaded single bearings with low load; depending on the respective application, higher or lower speed limits may apply in practice.
** For use with oil lubrication, these bearings are also available without shields.
Subject to change due to technical improvement.





Spindle ball bearings

GRW designation	Ma	in dimensior [mm] [inch]	ns in	Load r acc. to l	ratings DIN ISO		Ball set	Limiting s	peeds*		Preloa	d
Basic symbols	d	D	В	C _{or} [N]	C, [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) medium [N]	(S) heavy [N]
AC bearings, open, m	etric											
SV7203 C TA	17.00 .6693	40.00	12.00 .4724	5090	8730	12	5.556 .2187	85,000	55,000	35	70	140
SV7203 E TA	17.00	40.00	12.00	4860	8340	12	5.556	75,000	49,000	60	120	240
SV7804 C TA	.6693 20.00	1.5748 32.00	.4724 7.00	2772	3772	18	.2187 3.175	65,000	54,000	19	58	11.
HYSV7804 C TA	.7874 20.00	1.2598 32.00	.2756 7.00	1941	3772	18	.1250 3.175	96,000	69,000	19	58	11.
SV7804 E TA	.7874 20.00	1.2598 32.00	.2756 7.00	2870	3865	18	.1250 3.175	56,000	46,000	19	58	11.
	.7874	1.2598	.2756				.1250					
HYSV7804 E TA	20.00 .7874	32.00 1.2598	7.00 .2756	2009	3772	18	3.175 .1250	82,000	59,000	19	58	11
SV7904 C TA	20.00 .7874	37.00 1.4567	9.00 .3543	4854	7543	15	4.763 .1875	6,0000	49,000	39	116	23
HYSV7904 C TA	20.00 .7874	37.00 1.4567	9.00 .3543	3398	7543	15	4.763 .1875	88,000	63,000	39	116	23
SV7904 E TA	20.00	37.00	9.00	4554	7214	15	4.763	51,000	42,000	39	116	23
HYSV7904 E TA	.7874 20.00	1.4567 37.00	.3543 9.00	3188	7214	15	.1875 4.763	75,000	54,000	39	116	23
SV7004 C TA	.7874 20.00	1.4567 42.00	.3543 12.00	6090	9660	14	.1875 5.556	75,000	49,000	35	70	14
SV7004 E TA	.7874 20.00	1.6535 42.00	.4724 12.00	5810	9210	14	.2187 5.556	66,000	43,000	55	110	22
SV7204 C TA	.7874 20.00	1.6535 47.00	.4724 14.00	7320	11700	13	.2187 6.350	72,000	47,000	45	90	18
	.7874	1.8504	.5512				.2500					
SV7204 E TA	20.00 .7874	47.00 1.8504	14.00 .5512	7010	11100	13	6.350 .2500	63,000	41,000	70	140	28
SV7805 C TA	25.00 .9843	37.00 1.4567	7.00 .2756	2335	3397	19	3.175 .1250	55,000	45,000	17	52	10
HYSV7805 C TA	25.00 .9843	37.00 1.4567	7.00 .2756	1634	3397	19	3.175	81,000	58,000	17	52	10
SV7005 C TA	25.00 .9843	47.00 1.8504	12.00 .4724	6918	11769	12	6.747 .2656	47,000	39,000	59	177	35
HYSV7005 C TA	25.00	47.00	12.00	4843	11769	12	6.747	69,000	5,0000	59	177	35
SV7005 E TA	.9843 25.00	1.8504 47.00	.4724 12.00	6890	9920	16	.2656 5.556	57,000	37,000	55	110	22
(SV)7205 C TA	.9843 25.00	1.8504 52.00	.4724 15.00	8710	12800	15	.2187 6.350	63,000	41,000	50	100	20
(SV)7205 E TA	.9843 25.00	2.0472 52.00	.5906 15.00	8330	12100	15	.2500 6.350	55,000	36,000	80	160	32
(SV)7006 C TA	.9843 30.00	2.0472 55.00	.5906 13.00	9010	12100	17	.2500 5.953	55,000	36,000	40		
	1.1811	2.1654	.5118				.2344					
(SV)7006 E TA	30.00 1.1811	55.00 2.1654	13.00 .5118	8560	11500	17	5.953 .2344	48,000	31,000	65	130	260

GRW designation	Ma	in dimension [mm] [inch]	is in	Load r acc. to [I	Ball set	Limiting s	peeds*		Preloa	Ь
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) nedium [N]	(S) heavy [N]
C bearings, open, in	ch											
SV3/16 C TA	4.763	12.700	3.967	312	913	8	2.381	195,000	161,000	5	14	2
	.1875	.5,000	.1562				.0937					
HYSV3/16 C TA	4.763	12.700	3.967	218	913	8	2.381	287,000	206,000	5	14	2
	.1875	.5,000	.1562				.0937					
SV3/16 D TA	4.764	12.800	3.967	293	873	8	2.381	166,000	136,000	5	14	2
	.1876	.5039	.1562				.0937					
HYSV3/16 D TA	4.765	12.900	3.967	205	873	8	2.381	244,000	175,000	5	14	2
	.1876	.5079	.1562				.0937					
SV1/4AC TA	6.350	15.875	4.978	421	1114	9	2.500	153,000	126,000	6	17	6.0
	.2500	.6250	.1960				.0984					
HYSV1/4A C TA	6.350	15.875	4.978	295	1114	9	2.500	225,000	162,000	6	17	3
	.2500	.6250	.1960				.0984					
SV1/2/001 C TA	12.700	28.575	7.938	2063	4066	12	3.969	82,000	68,000	20	61	12
	.5,000	1.1250	.3125				.1563					
HYSV1/2/001 C TA	12.700	28.575	7.938	1444	4066	12	3.969	121,000	87,000	20	61	12
	.5,000	1.1250	.3125				.1563					
AC bearings. dismou	ntable. me	etric and in	ch									
SV784 D L2T	4.00	9.00	2.50	132	457	7	1.588	242,000	199,000	5	8	1
0,7,0,1,0,121	.1575	.3543	.0984	102	,		.0625	2.2,000	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Ŭ	0	
HYSV784 D L2T	4.00	9.00	2.50	94	457	7	1.588	355,000	256,000	5	8	1
	.1575	.3543	.0984				.0625	,	,			
SV725 C L2T	5.00	16.00	5.00	737	1626	9	2.500	157,000	130,000	8	24	4
	.1969	.6299	.1969				.0984					20
HYSV725 C L2T	5.00	16.00	5.00	515	1626	9	2.500	231,000	167,000	8	24	Z
	.1969	.6299	.1969				.0984					
SV725 D L2T	5.00	16.00	5.00	737	1626	9	2.500	134,000	110,000	8	24	1
	.1969	.6299	.1969				.0984				Part for	SUTE
HYSV725 D L2T	5.00	16.00	5.00	515	1626	9	2.500	197,000	142,000	8	24	2
	.1969	.6299	.1969				.0984					
SV707 C L2T	7.00	19.00	6.00	1183	2617	10	3.175	127,000	105,000	13	40	8
	.2756	.7480	.2362		10		.1250					
HYSV707 C L2T	7.00	19.00	6.00	828	2617	10	3.175	187,000	135,000	13	40	8
	.2756	.7480	.2362				.1250					
SV7000 C L2T	10.00	26.00	8.00	2550	4906	10	4.763	94,000	78,000	28	85	17
	.3937	1.0236	.3150			Ð	.1875		Nº4	- AN	XV	
HYSV7000 C L2T	10.00	26.00	8.00	1785	4906	10	4.763	139,000	10,000	28	85	17
	.3937	1.0236	.3150				.1875					
SV1/8A D20 L2T	3.175	7.938	2.779	207	609	7	1.588	266,000	219,000	5	8	
	.1250	.3125	.1094				.0625	and	NDKC			
HYSV1/8A D20 L2T	3.175	7.938	2.779	144	609	7	1.588	392,000	282,000	5	8	1
	.1250	.3125	.1094				.0625					
SV1/8B D20 L2T	3.175	9.525	3.967	134	461	8	1.588	228,000	188,000	5	10	2
	.1250	.3750	.1562				.0625	MAY .				
HYSV1/8B D20 L2T	3.175	9.525	3.967	95	461	8	1.588	336,000	242,000	5	10	2
	.1250	.3750	.1562				.0625					

GRW designation	Ma	in dimension [mm] [inch]	is in	Load r acc. to [B	Ball set	Limiting s	peeds*		Preloa	4
Basic symbols	d	D	В	C _{or} [N]	C, [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
C bearings, open, in	ch											
SV3/16 C TA	4.763 .1875	12.700 .5,000	3.967 .1562	312	913	8	2.381 .0937	195,000	161,000	5	14	28
HYSV3/16 C TA	4.763 .1875	12.700 .5,000	3.967 .1562	218	913	8	2.381 .0937	287,000	206,000	5	14	28
SV3/16 D TA	4.764 .1876	12.800 .5039	3.967 .1562	293	873	8	2.381 .0937	166,000	136,000	5	14	28
HYSV3/16 D TA	4.765 .1876	12.900 .5079	3.967 .1562	205	873	8	2.381 .0937	244,000	175,000	5	14	28
SV1/4A C TA	6.350 .2500	15.875 .6250	4.978 .1960	421	1114	9	2.500 .0984	153,000	126,000	6	17	34
HYSV1/4A C TA	6.350 .2500	15.875 .6250	4.978 .1960	295	1114	9	2.500 .0984	225,000	162,000	6	17	34
SV1/2/001 C TA	12.700 .5,000	28.575 1.1250	7.938 .3125	2063	4066	12	3.969 .1563	82,000	68,000	20	61	121
HYSV1/2/001 C TA	12.700 .5,000	28.575 1.1250	7.938 .3125	1444	4066	12	3.969 .1563	121,000	87,000	20	61	121
AC bearings. dismou	ntable. me	etric and in	ch									
SV784 D L2T	4.00 .1575	9.00 .3543	2.50 .0984	132	457	7	1.588 .0625	242,000	199,000	5	8	15
HYSV784 D L2T	4.00 .1575	9.00 .3543	2.50 .0984	94	457	7	1.588 .0625	355,000	256,000	5	8	15
SV725 C L2T	5.00 .1969	16.00 .6299	5.00 .1969	737	1626	9	2.500 .0984	1 <i>57</i> ,000	130,000	8	24	49
HYSV725 C L2T	5.00 .1969	16.00 .6299	5.00 .1969	515	1626	9	2.500 .0984	231,000	167,000	8	24	49
SV725 D L2T	5.00 .1969	16.00 .6299	5.00 .1969	737	1626	9	2.500 .0984	134,000	110,000	8	24	49
HYSV725 D L2T	5.00 .1969	16.00 .6299	5.00 .1969	515	1626	9	2.500 .0984	197,000	142,000	8	24	49
SV707 C L2T	7.00 .2756	19.00 .7480	6.00 .2362	1183	2617	10	3.175 .1250	127,000	105,000	13	40	80
HYSV707 C L2T	7.00 .2756	19.00 .7480	6.00 .2362	828	2617	10	3.175 .1250	187,000	135,000	13	40	80
SV7000 C L2T	10.00 .3937	26.00 1.0236	8.00 .3150	2550	4906	10	4.763 .1875	94,000	78,000	28	85	170
HYSV7000 C L2T	10.00 .3937	26.00 1.0236	8.00 .3150	1785	4906	10	4.763 .1875	139,000	10,000	28	85	170
SV1/8A D20 L2T	3.175 .1250	7.938 .3125	2.779 .1094	207	609	7	1.588 .0625	266,000	219,000	25	8	16
HYSV1/8A D20 L2T	3.175 .1250	7.938 .3125	2.779 .1094	144	609	7	1.588 .0625	392,000	282,000	5	8	16
SV1/8B D20 L2T	3.175 .1250	9.525 .3750	3.967 .1562	134	461	8	1.588 .0625	228,000	188,000	5	10	20
HYSV1/8B D20 L2T	3.175	9.525	3.967	95	461	8	1.588	336,000	242,000	5	10	20

* The indicated speed limits are guide values for spring-loaded single bearings with low load; depending on the respective application, higher or lower speed limits may apply in practice.
** For use with oil lubrication, these bearings are also available without shields.
Subject to change due to technical improvement.





Spindle ball bearings

GRW designation	Mc	iin dimension [mm] [inch]	ns in	Load r acc. to [I	Ball set	Limiting s	peeds*		Preloa	Ч
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) medium [N]	(S) heavy [N]
AC bearings, sealed, i	metric											
SV725A-2VZ C TA	5.00 .1969	16.00 .6299	5.00 .1969	647	1305	12	1.984 .0781	194,000**	155,000	7	20	4(
HYSV725A-2VZ C TA	5.00 .1969	16.00 .6299	5.00 .1969	453	1305	12	1.984 .0781	290,000**	194,000	7	20	40
SV725A-2VZ E TA	5.00 .1969	16.00 .6299	5.00 .1969	607	1248	12	1.984 .0781	165,000**	132,000	7	20	4
SV788B-2VZ C TA	8.00 .3150	16.00 .6299	4.00 .1575	723	1374	13	1.984 .0781	174,000**	139,000	7	21	4
HYSV788B-2VZ C TA	8.00 .3150	16.00 .6299	4.00 .1575	506	1374	13	1.984 .0781	261,000**	174,000	7	21	4
SV708B-2VZ C TA	8.00 .3150	22.00 .8661	7.00 .2756	1298	2625	10	3.175 .1250	144,000**	115,000	13	40	8
HYSV708B-2VZ C TA	8.00 .3150	22.00 .8661	7.00 .2756	909	2625	10	3.175 .1250	216,000**	144,000	13	40	8
SV708B-2VZ E TA	8.00 .3150	22.00 .8661	7.00 .2756	1218	2510	10	3.175 .1250	122,000**	98,000	13	40	8
HYSV708B-2VZ E TA	8.00 .3150	22.00 .8661	7.00 .2756	853	2510	10	3.175 .1250	183,000**	122,000	13	40	8
SV709A-2VZ C TA	9.00 .3543	24.00 .9449	7.00 .2756	1493	2822	11	3.175 .1250	128,000**	102,000	14	43	8
HYSV709A-2VZ C TA	9.00 .3543	24.00 .9449	7.00 .2756	1045	2822	11	3.175 .1250	191,000**	128,000	14	43	8
SV7800A-2VZ C TA	10.00 .3937	19.00 .7480	5.00 .1969	876	1487	15	1.984 .0781	143,000**	114,000	8	23	4
HYSV7800A-2VZ C TA	10.00 .3937	19.00 .7480	5.00 .1969	613	1487	15	1.984 .0781	215,000**	143,000	8	23	4
SV7900B-2VZ C TA	10.00 .3937	22.00 .8661	6.00 .2362	1173	2047	13	2.500 .0984	128,000**	102,000	11	33	6
HYSV7900B-2VZ C TA	10.00 .3937	22.00 .8661	6.00 .2362	821	2047	13	2.500 .0984	192,000**	128,000	11	33	6
SV7000A-2VZ C TA	10.00 .3937	26.00 1.0236	8.00 .3150	2030	3879	10	3.969 .1563	115,000**	92,000	20	60	12
SV7000A-2VZ E TA	10.00 .3937	26.00 1.0236	8.00 .3150	1905	3710	10	3.969 .1563	98,000**	78,000	20	60	12
HYSV7000A-2VZ E TA	10.00 .3937	26.00 1.0236	8.00 .3150	1334	3710	10	3.969 .1563	147,000**	98,000	20	60	12
SV7901A-2VZ C TA	12.00 .4724	24.00 .9449	6.00 .2362	1478	2329	16	2.500 .0984	115,000**	92,000	12	35	7
HYSV7901A-2VZ C TA	12.00 .4724	24.00 .9449	6.00 .2362	1035	2329	16	2.500 .0984	173,000**	115,000	12	35	7
SV7901A-2VZ E TA	12.00 .4724	24.00 .9449	6.00 .2362	1387	2227	16	2.500 .0984	98,000**	79,000	12	35	7
HYSV7901A-2VZ E TA	12.00 .4724	24.00 .9449	6.00 .2362	971	2227	16	2.500 .0984	147,000**	98,000	12	35	7
SV7001B-2VZ C TA	12.00 .4724	28.00 1.1024	8.00 .3150	2328	3603	16	3.175 .1250	101,000**	80,000	18	55	11
HYSV7001B-2VZ C TA	12.00 .4724	28.00 1.1024	8.00 .3150	1141	3603	16	3.175 .1250	151,000**	101,000	18	55	11
SV7001B-2VZ E TA	12.00 .4724	28.00 1.1024	8.00 .3150	2184	3446	16	3.175 .1250	85,000**	68,000	18	55	11

GRW designation	Ma	iin dimensior [mm] [inch]	ns in	Load r acc. to l	atings DIN ISO		Ball set	Limiting s	peeds*		Preloa	
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light r [N]	(M) nedium [N]	(S) heav [N]
C bearings, sealed,	metric											
HYSV7001B-2VZ E TA	12.00	28.00	8.00	1070	3446	16	3.175	128,000**	85,000	18	55	11
	.4724	1.1024	.3150				.1250					
SV7201B-2VZ E TA	12.00	32.00	10.00	3034	5373	11	4.763	80,000**	64,000	29	86	17
	.4724	1.2598	.3937				.1875					
HYSV7201B-2VZ E TA	12.00	32.00	10.00	1487	5373	11	4.763	120,000**	80,000	29	86	17
	.4724	1.2598	.3937				.1875					
SV7902A-2VZ C TA	15.00	28.00	7.00	2359	3586	16	3.175	95,000**	76,000	18	55	1
	.5906	1.1024	.2756				.1250					
HYSV7902A-2VZ C TA	15.00	28.00	7.00	1651	3586	16	3.175	143,000**	95,000	18	55	1
	.5906	1.1024	.2756				.1250					
SV7902A-2VZ E TA	15.00	28.00	7.00	2213	3430	16	3.175	81,000**	65,000	18	55	1
	.5906	1.1024	.2756				.1250	,	,			
HYSV7902A-2VZ E TA	15.00	28.00	7.00	1549	3430	16	3.175	121,000**	81,000	18	55	1
	.5906	1.1024	.2756				.1250	,	,			
SV7002A-2VZ C TA	15.00	32.00	9.00	3337	5125	15	3.969	87,000**	70,000	26	79	1
017 002/12/2 0 1/1	.5906	1.2598	.3543	0007	0120	10	.1563	0,,000	, 0,000	20	, ,	
HYSV7002A-2VZ C TA	15.00	32.00	9.00	2336	5125	15	3.969	131,000**	87,000	26	79	1
11017002/1212 C 1/1	.5906	1.2598	.3543	2000	5125	10	.1563	101,000	07,000	20		'
SV7002A-2VZ E TA	15.00	32.00	9.00	3131	4902	15	3.969	74,000**	59,000	26	79	1
JV/OUZAZVZ L TA	.5906	1.2598	.3543	5151	4902	IJ	.1563	74,000	39,000	20	/ 4	
HYSV7002A-2VZ E TA	15.00	32.00	9.00	2192	4902	15	3.969	111,000**	74,000	26	79	1
III JV/ OUZA-ZVZ L IA	.5906	1.2598	.3543	2192	4902	IJ	.1563	111,000	74,000	20	/ 4	
SV7903A-2VZ C TA	17.00	30.00	7.00	2402	3554	16	3.175	88,000**	70,000	18	55	1
307903A-202 C IA	.6693	1.1811	.2756	2402	3334	10	.1250	00,000	70,000	10	55	
HYSV7903A-2VZ C TA	17.00	30.00	7.00	1682	3554	16	3.175	132,000**	88,000	18	55	1
113V/903A-2VZ C IA	.6693	1.1811	.2756	1002	3334	10	.1250	132,000	00,000	10	55	
		30.00	7.00	2054	3399	16	3.175	75.000**	40.000	10	EE	1
SV7903A-2VZ E TA	17.00			2254	3399	10		75,000**	60,000	18	55	
	.6693	1.1811	.2756	1.570	3399	1 /	.1250	110.000**	75.000	10		1
HYSV7903A-2VZ E TA	17.00	30.00	7.00	1578	3399	16	3.175	112,000**	75,000	18	55	1
	.6693	1.1811	.2756	4.41.5	1151	11	.1250	15000**	54.000	0.4	100	0
SV7003-2VZ C TA	17.00	35.00	10.00	4415	6654	14	4.763	65,000**	54,000	34	102	2
	.6693	1.3780	.3937	0001	1154	1.4	.1875	0(000 **	(0.000	0.4	100	-
HYSV7003-2VZ C TA	17.00	35.00	10.00	3091	6654	14	4.763	96,000**	69,000	34	102	2
	.6693	1.3780	.3937	12.40			.1875				100	-
SV7003-2VZ E TA	17.00	35.00	10.00	4143	6363	14	4.763	56,000**	46,000	34	102	20
	.6693	1.3780	.3937			ŧ.	.1875		North	2857	$\overline{\mathcal{M}}$	ΔI
HYSV7003-2VZ E TA	17.00	35.00	10.00	2900	6363	14	4.763	82,000**	59,000	34	102	2
	.6693	1.3780	.3937				.1875					
SV7904A-2VZ C TA	20.00	37.00	9.00	3868	5394	16	3.969	70,000	56,000	27	81	A,
	.7874	1.4567	.3543				.1563	1/ B	NPKC			
HYSV7904A-2VZ C TA	20.00	37.00	9.00	2708	5394	16	3.969	105,000	70,000	27	81	10
	.7874	1.4567	.3543				.1563					
SV7005A-2VZ C TA	25.00	47.00	12.00	7909	10661	17	5.556	56,000	44,000	53	160	3
	.9843	1.8504	.4724				.2187	PHO I				
HYSV7005A-2VZ C TA	25.00	47.00	12.00	5536	10661	17	5.556	83,000	56,000	53	160	32
	.9843	1.8504	.4724				.2187					

* The indicated speed limits are guide values for spring-loaded single bearings with low load; depending on the respective application, higher or lower speed limits may apply in practice.
 ** For use with oil lubrication, these bearings are also available without shields.
 Subject to change due to technical improvement.





Profiled rollers

Profiled rollers are double-row ball bearings, which are able to accept axial loads in both directions, as well as high radial loads. Usually, the contact surface is shaped like a Gothic arch; contact surface and shaft touch each other in two zones.

On request, other contour surface designs are available (e.g. V groove, spherical outer ring, etc.).

Inner and outer rings can be made of chrome steel 100Cr6 or corrosion-resistant chrome steels X65Cr13 or X30CrMoN 15-1. Balls can be made of chrome steel 100Cr6, X65Cr13 or ceramic.

GRW profiled rollers have non-contact shields. On request, contact seals (e.g. Teflon[®], NBR) are available as an alternative. The rollers are lubricated for life and are also available with FDA-approved or autoclavable lubricants.

For further information please contact your nearest GRW Sales Representative.



σ

Profile roller with inner ring extended on both sides

Bearing units

Bearing units are complete pre-mounted assemblies, comprising of at least one ball bearing, shaft or housing, optional spacers, shims or spring washers.

GRW assembles the components in bearing units primarily by using adhesives. Backlash free bearing units are produced cost effectively by precisely gluing the bearings under an axial pre-load. GRW has engineered special gluing equipment and techniques to ensure high accuracy and strength.

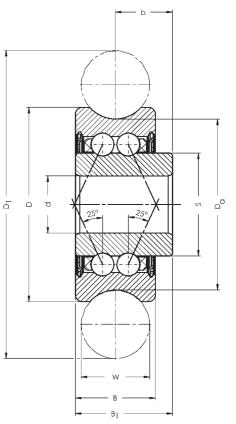
When using GRW bearing units, customers will profit by following benefits:

- Cost advantages by eliminating possibility of improper customer assembly.
- Pre-mounted units are easier to handle than single bearings, reducing stock control.
- At GRW the bearings are mounted in a clean room under optimum conditions.

GRW designation	Drawing no.	d	D _a	D	D	w	В	B ₁	ь	S
687/603282-2RZ	604623	5	_	17	27	6	7	8	4	9
687/603282-2Z	603282	5	-	17	27	6	7	8	4	9
687/602057-2Z	602057	5	-	17	25	5	7	8.5	5	9
687/601938-2Z	601938	5	-	17	27	6	7	8.5	5	9
687/601935-2Z	602055	5	_	16	22	4	7	8.5	5	9
687/601935-2Z	601935	5	-	16	22	4	7	8.5	5	9
608/602030-2ZF	604976	8	_	24	34	6	11	11	5.5	11.8
608/602030-2ZF	602030	8	-	24	34	6	11	11	5.5	11.8
608/602024-2ZF	602024	8	-	24	37	8	11	12.5	7	11.8
608/601947-2ZF	602053	8	-	24	34	6	11	12.5	7	11.8
608/601947-2ZF	601947	8	-	24	34	6	11	12.5	7	11.8
6201/604947-2Z	604947	12	-	35	51.3	10	15.9	15.9	7.95	18.28

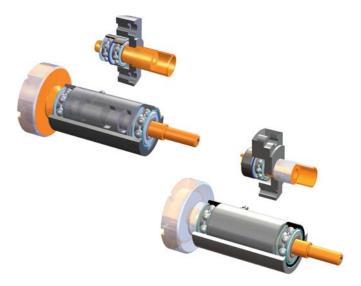
Subject to change due to technical improvement.





Profile roller with inner ring extended on one side

• Depending on the customer's requirements, other functional elements may be integrated into the bearing units, for example springs and seals or moulded tyres.





Thin-section bearings

Thin-section bearings are bearings with very thin ring cross-sections (light ISO dimension series 67/68) or bearings of identical cross-sections, independent of their bore diameter (inch series: Extra Thin Series, Thin Series).

In addition to their small footprint and low weight, they are characterised by low torque and high rigidity.

Thin-section bearings are available in the following versions: open (standard), with closures, with an extended inner ring, with a flanged outer ring and as an angular contact or full-complement bearing at a maximum outside diameter of 40 mm.

The closures are available in -2Z and -2TS versions. As standard, thin-section bearings are all ABEC5.

Contact us regarding other available versions (e.g. Superduplex) ABEC7, and ABEC9.



GRW	d	l	D)	I	В	r,	min	d	min	ď	max	D	max
designation	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]
15875A	15.875	.625	22.225	.875	3.967	.156	0.25	.010	16.9	.665	17.9	.705	20.6	.811
15875A-2Z	15.875	.625	22.225	.875	4.978	.196	0.25	.010	16.9	.665	17.9	.705	20.6	.811
15875A-2TS	15.875	.625	22.225	.875	4.978	.196	0.25	.010	16.9	.665	17.2	.677	20.6	.811
19050A	19.050	.750	25.400	1.000	3.967	.156	0.25	.010	20.1	.791	21.1	.831	23.7	.933
19050A-2Z	19.050	.750	25.400	1.000	4.978	.196	0.25	.010	20.1	.791	21.1	.831	23.7	.933
19050A-2Z	19.050	.750	25.400	1.000	4.978	.196	0.25	.010	20.1	.791	20.4	.803	23.7	.933
22225A	22.225	.875	28.575	1.125	3.967	.156	0.25	.010	23.3	.917	24.3	.957	26.9	1.059
22225A-2Z	22.225	.875	28.575	1.125	4.978	.196	0.25	.010	23.3	.917	24.3	.957	26.9	1.059
22225A-2TS	22.225	.875	28.575	1.125	4.978	.196	0.25	.010	23.3	.917	23.6	.929	26.9	1.059
26988A	26.988	1.063	33.338	1.313	3.967	.156	0.25	.010	28.1	1.106	29. 1	1.146	31.7	1.248
26988A-2Z	26.988	1.063	33.338	1.313	4.978	.196	0.25	.010	28.1	1.106	29. 1	1.146	31.7	1.248
26988-2TS	26.988	1.063	33.338	1.313	4.978	.196	0.25	.010	28.1	1.106	28.4	1.118	31.7	1.248
31750A	31.750	1.250	38.100	1.500	3.967	.156	0.25	.010	32.8	1.291	33.8	1.331	36.4	1.433
31750A-2Z	31.750	1.250	38.100	1.500	4.978	.196	0.25	.010	32.8	1.291	33.8	1.331	36.4	1.433
31750A-2TS	31.750	1.250	38.100	1.500	4.978	.196	0.25	.010	32.8	1.291	33.1	1.303	36.4	1.433
34925A	34.925	1.375	41.275	1.625	3.967	.156	0.25	.010	36.0	1.417	37.0	1.457	39.5	1.555
34925A-2Z	34.925	1.375	41.275	1.625	4.978	.196	0.25	.010	36.0	1.417	37.0	1.457	39.5	1.555
34925A-2TS	34.925	1.375	41.275	1.625	4.978	.196	0.25	.010	36.0	1.417	36.3	1.429	39.5	1.555

Subject to change due to technical improvement.

Hybrid and full ceramic ball bearings

Conventional ball bearings are limited when operating at high temperatures. in a vacuum. or in a corrosive environment. All ceramic bearings have proven to be ideally suited for these extreme applications.

Zirconium oxide (ZrO_2) and silicon nitride (Si_3N_4) are typical materials used in all ceramic bearings. which provide excellent corrosion and temperature resistance as well as other mechanical properties.

Material properties:

Properties	Unit	Si₃N₄ HY	ZrO ₂ ZO
Density	g/cm³	3.2	6.05
Hardness	HRC	> 75	> 69
E module	GPa	320	200
Poisson coefficient		0.26	0.2
Linear expansion coefficient	x10-6 K-1	2.9	10
Max. temperature	°C	800	600
Corrosion resistance		very good	good
Electrical conductivity		Insulator	Insulator





High chemical resistance

All ceramic ball bearings have specific advantages for applications with mixed-friction because they remain operative for a longer period of time than conventional steel bearings even in the case of lube deprivation.

Corrosion resistance

All ceramic bearings resist cold micro welding to other materials which allows for particularly low adhesive wear. Certain applications make use of conventional bearings almost impossible. For example: chemical resistance of all ceramic bearings to corrosive materials allows usage in chemical applications.

Thermal expansion

Full ceramic bearings will remain dimensionally stable even at high temperature fluctuations.

Non-magnetism and electrical insulation

The non-magnetic properties of the ceramic materials prevent interference with magnetic fields and the ceramic acts as an insulator preventing current flow.

Extra-duplex bearings

Tandem-duplex bearings

Extra-duplex bearings are double-row deep groove radial bearings or angular contact ball bearings with a split inner or outer ring. One floating ring is accurately preloaded and then

or changes in axial preload during assembly.

Special ball bearings

GRW develops and produces a complete range of custom bearing options.

Superduplex bearings

Superduplex bearings are also known as double row deep-groove ball bearings or angular contact ball bearings featuring split inner or outer rings. One of the ring sets, either outer or inner, consists of a double row integral set of raceways.

Its compact design permits easy handling and assembly. The inner or outer split rings are paired according to customer specifications ensuring that GRW bearings will meet the required axial preload.

groove bearings. The raceways are extremely close to each other (in the micron range). These bearings are designed to handle both radial loads and axial loads in one direction by ensuring that the load is evenly distributed to all balls.

Bearings with custom outer geometries

GRW can produce single or double-row bearings with a spherical or grooved outer ring and also can provide moulded and plastic rubber types.

www.grw.de



Bearing and shaft can be combined to provide an integrated assembly. In this design the raceway is ground on the shaft and the bearing assembly is delivered completely assembled ready to use.

Customised outer geometries and moulded plastic or rubber tyres can be supplied upon request.

Bearing/ housing assemblies

For these special designs, the raceway of the outer ring is ground directly into the housing. Complex housings, flanges and threaded mounting holes maintain the tight tolerances necessary for proper installation.

Precision Components

GRW manufactures precision spacers and precision components that incorporate threads, steps, grooves, bores, etc. to tolerances in the micron (μ) range.





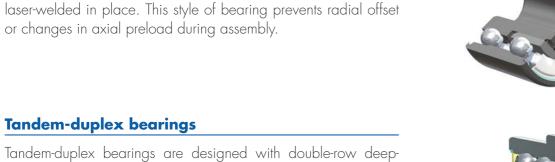








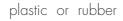




























Coated bearings

Sometimes it is not possible to use conventional lubricants especially in applications that are exposed to extremely high or low temperatures, ultra high vacuum, or in close proximity to optical systems.

The solution in these cases may be special coatings of gold, silver, MoS_2 , or Teflon[®]. These thin layers act as a dry film lubricant. Development of this technology has made applications possible even at temperatures of -70 °C to +400 °C or in a high vacuum.

Protection against wear is also an advantage of using thin coated bearings. Raceways, bearing bores and/or outer surfaces can be thinly coated to meet each application's requirements. Possible uses for these types of coatings are rollers, paper cutting blade wheels, bearings used in chemical or food processing industries, and medical instruments.

As each coating can be applied by a variety of technologies, GRW will work with each customer to select the optimum coating process to meet the application requirements.



EXTREME







GRW goes EXTREME

GRW goes EXTREME - this is how our experts describe production beyond our standard product offerings: individually adapted, customised "tuning" of ball bearings for extreme applications.

With the new program EXTREME, GRW is trail blazing new paths.

High-Speed

- The EXTREME solution:
- Highest precision
- Ceramic balls
- Use of special retainers
- Optimum bearing design



EXTREME shows what we are planning to achieve with these products, and how we are reaching these goals. Ball bearings of the EXTREME series offer added value for almost all types of applications. Join us in the EXTREME world of GRW.

Resistance to aggressive media

Selecting the right material is paramount if you need the highest resistance to corrosion or when aggressive media is specified. The EXTREME solution:

- Rings made of SV-30 or use corrosion resistant coatings
- Ceramic balls
- Acid and alkali-proof synthetic retainers

Extreme heat up to +450 °C

The EXTREME solution:

- High-temperature chrome steels
- High-temperature retainers or full complement designs
- Dry-film lubricated designs



Non-magnetic solutions

GRW ball bearings with non-magnetic properties.

The EXTREME solution:

- Rings made from a cobalt-based alloy with a hardness of up to 59 HRC
- Ceramic balls
- Retainer made from a non-magnetic material







EXTREME



Easy solutions that can withstand the highest loads

The EXTREME solution:

- Optimum dimensioning of ball size and curvature
- For optimised load ratings and rigidity
- Multi-row bearing systems



Requirements in a vacuum

Ball bearing applications in space / in vacuum environments.

The EXTREME solution:

- Use of special materials
- Surface treatments
- Special lubrications



Resistance ensured down to absolute zero

The EXTREME solution:

- Special retainer materials
- Use of special lubricants
- Coatings



GRW's special product range EXTREME

Highest material quality

The GRW portfolio lists many different ring materials that can meet all special requirements in:

- Hardness,
- Rolling resistance,
- Corrosion resistance,
- Heat resistance and L-10 life,
- Non-magnetic requirements.

Perfect lubrication

100% performance in extreme applications requires extreme materials, absolute precision and cleanliness. For this reason, GRW relies on the experience of their engineers and technicians when selecting the materials – and on internal results from our own chemistry laboratory.

The correct lubricant is of high relevance. It has a major effect on:

- Bearing friction
- Running noise
- Limiting speeds
- L-10 life ratings

GRW's wide selection of high-quality greases and oils has the exacting solution for every extreme application. Our recommended lubricants are based upon manufacturer data as well as in house tests results obtained from our proprietary test facility. From lubricants for high-speed applications to lubricants that are resistant to aggressive sterilisation processes – GRW offers a customised solution tailored to your individual needs.

Special low-torque bearings

Special low-torque bearings in the field of measurement and control engineering operate reliably and precisely even when running dry.

These ball bearings meet the highest demands in bearing engineering:

- Minimum starting and dynamic torque
- Repeatable low friction torque

EXTREME



Retainers for practically any application

In addition to the standard retainer made from corrosion resistant steel, GRW has a range of widely different synthetic materials for selecting the suitable solution for each customer's specific application.

Patented know-how

GRW has proven expertise in the field of ball bearing retainers, supported by a number of patents.

Maximizing load ratings and limiting speeds

From the start, optimisation measures are considered for their potential to maximize the static and dynamic radial load ratings or limiting speeds of each ball bearing. Further optimisation measures are taken into account for internal geometries as well, i.e. pitch circle diameter, curvature, ball diameter and ball complement, material, tolerance and finally manufacturing technology of bearing components.

Turbine ball bearings by a factor of 5

Turbine ball bearings used in dental handpieces, utilise a new type of retainer material that achieves a factor of 5 increase in life compared to standard bearings equipped with retainers made from commercially available synthetics.

Manufacturers using ball bearings with the new retainer materials can offer their customers:

- Increased performance and fewer in-warranty returns
- improved durability despite improper handling of the device, e.g. improper oil maintenance.

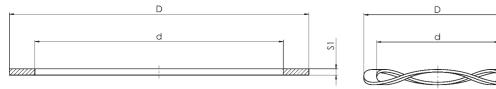
Tested quality

GRW's in-house test facility is the core element of their research and development. The suitability of a synthetic material is evaluated on their proprietary, fully automated equipment for properties such as wear and elasticity, additional functionality and life-testing allow them to optimise the performance of each ball bearing for individual customer's specific requirements.

For further information, please contact your nearest GRW sales representative.



Accessories



Shims AS

Shims are often used to balance the accumulation of tolerances (tolerance chains) and axial tolerances.

GRW spring washers are made of corrosion-resistant 1.4310 (AISI 301) spring wire. They are heat-treated, burr-free, and have an extremely fine surface finish.

Spring washers WF

Spring washers are used for defined axial preloading of bearings, particularly for miniature and small ball bearings. The manufacture of these spring washers includes cutting and punching processes. Through a subsequent finishing process they can be calibrated to provide highly accurate preload tolerances as required for special applications.

GRW spring washers are made of corrosion-resistant 1.4310 (AISI 301) spring wire. They are heat-treated, burr-free, and have an extremely fine surface finish. Our spring washers are designed with 3 waves ensuring even support of the bearing during axial preloading.

Shims		Dimensions [mm] Spring washers		for use in	ion
d x D	5	spring wasners (d x D x H x s)	Spring constant	for use on the shaft	for use in the housing
		(0 × 0 × 11 × 3)	[N/mm]		
AS 1.55 x 2.50	0.15	– WF 1.60 x 2.90 x 0.40 x 0.06	- 50.0	68/1,5,69/1,5	_
	_	WF 1.90 x 2.80 x 0.50 x 0.08	60.0		
AS 2.00 x 4.30	0.10 0.16	_	_	_	_
AS 2.25 x 3.20	0.20	WF 2.15 x 3.10 x 0.50 x 0.08	54.9	682, 692, 5/64	
AS 2.80 x 3.90	0.10 0.08 0.10	WF 2.70 x 3.80 x 0.50 x 0.08	52.0	60/2,5,68/2,5,69/2,5,3/32	68/1,5,691,1191
AS 3.05 x 4.50	0.10 0.16	_		_	_
AS 3.30 × 4.40	0.20 0.08 0.10 0.12	WF 3.20 × 4.30 × 0.50 × 0.10	32.5	623, 683, 693, 1/8A, 1/8B, 3175,1/8A/6, 1/8B/083	_
AS 3.50 x 5.00	0.08	_	-	-	_
AS 3.80 x 4.90	0.08 0.10 0.12	WF 3.70 x 4.80 x 0.55 x 0.10	32.0	_	682,69/1,5
AS 4.05 x 5.50	0.10 0.20	_	_	_	_
AS 4.30 x 5.85	0.10 0.12 0.15	WF 4.20 x 5.75 x 0.65 x 0.12	40.0	604, 624, 634, 684, 694, 3967	68/2,5,692
AS 4.90 x 6.20	0.10 0.12 0.15	WF 4.80 x 6.10 x 0.60 x 0.12	37.0	3/16, 4763A, 4763B	5/64, 3175
AS 5.20 x 6.75	0.15	_	_	_	_
AS 5.30 x 6.85	0.10 0.12 0.15	WF 5.20 x 6.75 x 0.65 x 0.12	22.0	625, 635, 685, 695	683, 69/2,5
AS 5.50 x 8.50	0.40	-	-	-	-
AS 6.30 x 7.85	0.12 0.15 0.18	WF 6.20 x 7.75 x 0.70 x 0.15	38.0	626, 686, 696	60/2,5, 693, 3/32, 1/8A, 3967, 4763A
AS 6.70 x 9.40	0.10	_	_	- /	
AS 7.30 x 8.80	0.12 0.15 0.18	WF 7.20 x 8.70 x 0.90 x 0.15	28.5	607, 627, 687, 697	684
_	-	WF 7.20 x 12.00 x 1.55 x 0.13	41.8	607, 627	6350B, 7938, 1/8B/08
AS 8.30 x 9.80	0.10 0.15 0.18 0.20	WF 8.20 x 9.70 x 0.85 x 0.18	26.0	608, 688, 698, 7938	623
AS 9.30 x 10.80	0.15 0.18 0.20	WF 9.20 x 10.70 x 1.15 x 0.18	22.0	609, 629, 689, 699	685, 694
AS 10.30 x 11.80	0.18 0.20	WF 10.20 x 11.70 x 1.05 x 0.20	18.5	6000, 6800, 6900,3/8	604
_	0.22	WF 10.50 x 15.80 x 1.85 x 0.25	77.0	6000	625, 634
AS 11.30 x 12.80	0.18 0.20 0.22	WF 11.20 x 12.70 x 1.30 x 0.20	16.0	- 6	624, 686, 695
AS 12.30 x 13.80	0.22 0.20 0.22 0.25	WF 12.20 × 13.70 × 1.30 × 0.22	20.0	- 386	687
AS 13.30 x 14.80	0.20 0.22 0.25	WF 13.20 x 14.70 x 1.30 x 0.22	13.0	-ACH	696
AS 14.35 x 15.80	0.22 0.25 0.30	WF 14.20 x 15.65 x 1.55 x 0.25	17.0	ACC ACC ACCA	625, 634, 688, 1/4A
AS 15.35 x 16.80	0.22 0.25 0.30	WF 15.20 x 16.65 x 1.55 x 0.25	14.5	CHEERS N	689, 697
AS 16.00 × 22.00	0.10 0.20	WF 15.80 x 21.80 x 1.60 x 0.20	10.0	ATTAN A	3/8
AS 16.40 x 18.80	0.25 0.30 0.35	WF 16.20 x 18.55 x 2.15 x 0.30	28.5	A B	607, 626, 635, 6800, 698, 1/4

Material 1.4310 (AISI 301). Before planning on the use of shims and spring washers, please ask about the availability. Subject to change due to technical improvement. Minimum quantity 100 pieces.



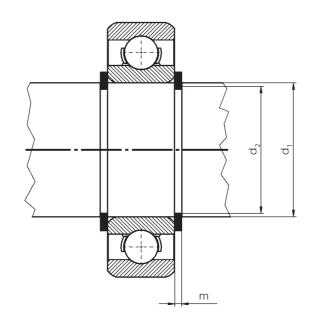


Accessories

Retaining rings – (shaft circlips WSR, bore retaining rings BSR)

Retaining rings are precision engineered components that are designed to be applied on shafts or in bores providing a shoulder that accurately positions, locates and retains parts of an assembly. They are especially useful with small and evenly distributed axial and radial loads. It is important to ensure that the face of the retaining ring does not touch the edge radius of the bearing. If the face does touch the radial edge, we recommend that you use our shims in conjunction with our retaining rings.

GRW retaining rings are constructed from cold-drawn spring wire 1.4310 (AISI 301), which exhibits an extremely constant cross section. They are corrosionresistant and free of any scale or burrs.



Assembly of a ball bearing with shaft circlips

Shaft circlips

Туре	Shaft	G	iro			
	d ₁	d ₃ max.	Split lock b ± 0.10	s ± 0.02	d ₂ - 0.05	m + 0.03
WSR 3	3	2.60	0.50	0.30	2.70	0.33
WSR 4	4	3.60	0.50	0.30	3.70	0.33
WSR 5	5	4.50	0.70	0.40	4.60	0.44
WSR 6	6	5.45	0.70	0.40	5.60	0.44
WSR 7	7	6.45	0.70	0.40	6.60	0.44
WSR 8	8	7.35	0.90	0.50	7.50	0.55
WSR 9	9	8.30	0.90	0.50	8.50	0.55
WSR 10	10	9.25	0.90	0.50	9.50	0.55

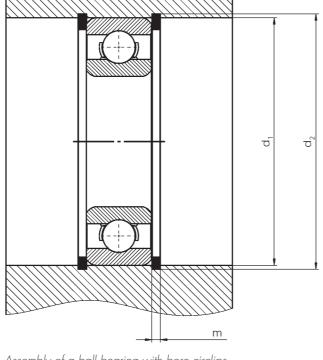
Material 1.4310 (AISI 301). Subject to change due to technical improvement. Packaging unit 1000 pieces.

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Bore circlips

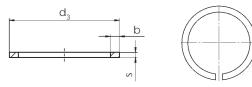
Туре	Shaft		Dimensi Split lock	ons [mm]	G	iro
	dı	d ₃ min.	b ± 0.10	s ± 0.02	d ₂ - 0.05	m + 0.03
BSR 4	4	4.40	0.50	0.30	4.30	0.33
BSR 5	5	5.45	0.50	0.30	5.30	0.33
BSR 6	6	6.45	0.50	0.30	6.30	0.33
BSR 7	7	7.50	0.50	0.30	7.30	0.33
BSR 8	8	8.60	0.70	0.40	8.40	0.44
BSR 9	9	9.60	0.70	0.40	9.40	0.44
BSR 10	10	10.65	0.70	0.40	10.40	0.44
BSR 11	11	11.65	0.70	0.40	11.40	0.44
BSR 12	12	12.75	0.90	0.50	12.50	0.55
BSR 13	13	13.75	0.90	0.50	13.50	0.55
BSR 14	14	14.80	0.90	0.50	14.50	0.55
BSR 15	15	15.80	0.90	0.50	15.50	0.55
BSR 16	16	16.85	0.90	0.50	16.50	0.55
BSR 17	17	17.85	0.90	0.50	17.50	0.55
BSR 19	19	20.00	1.10	0.60	19.60	0.66

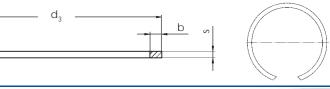
Material 1.4310 (AISI 301). Subject to change due to technical improvement. Packaging unit 1000 pieces.



Assembly of a ball bearing with bore circlips











Test engineering

Orakel III

Orakel III is an automated, stand-alone test module for performing cyclical loading tests on turbines and surgical handpieces. Quantifiable results are recorded while a LED continuously displays the current operating mode. The pneumatic load unit is calibrated and decelerates the test specimen with a force between 0.1 and 6 N at an accuracy of +/-0.1 N. An adjusting device allows continuous measurement of the test specimen.

While the magnetic speed sensor records speeds from 20,000 to 600,000 rpm, the instrument holder can be adjusted to any angle to accommodate all potential parameters. This module can be operated via a Windows PC (the PC is only required for operating purposes, the module tests independently).

Benefits:

- Up to 7,000 cycles can be executed without interruption.
- Uniform test processes can be exactly reproduced.
- The operation of the module only requires electric power and clean compressed air.
- Testing capacities can be expanded at any time by adding additional modules.
- Easy documentation: For each cycle, the measured speed is stored and can be written in a text file along with details of the completed testing time.
- Up to 10 modules can be controlled by one PC.



Note: Orakel III, the test module developed by GRW, is available for purchase. Contact us for price and availability!

Speedmaster

The GRW Speedmaster is a noncontact speedmeasuring device especially designed for high RPM rotating instruments used in the dental industry.

It may also be used for other high-speed applications such as motors or high-frequency spindles.



Note: Speedmaster, developed by GRW, is available for purchase. Contact us for price and availability!

This instrument consists of: the basic measuring unit, AC adapter, speed sensor, permanent magnet, a hard metal test probe for clamping in the dental instrument, and a measuring stand to hold the speed sensor.

Measurement Principle

A test probe or a motor shaft is magnetised by means of the attached permanent magnet. The sensor is positioned 1 and 10 mm away from the magnetised shaft. When the shaft rotates, the weak magnetic field is recorded by the special GRW sensor, then amplified and displayed in rpm, revolutions per minute.

The non-contact measurement is designed for speeds from 20,000 to 600,000 min⁻¹

The device has proven to be particularly useful in development and production as well as the repair of dental turbines and surgical handpieces.

GRW laboratory services

By analysing and testing materials in their own laboratory, GRW ensures the quality and future development of their products. GRW engineers and chemists work continuously to improve the rating life and efficiency of their ball bearings. Customers



FTIR spectroscopy with ATR technology for non-destructive analysis of the quality composition of organic materials.

GRW offers the following services:

General analytics, for example determination of Ha –

- Acid concentration
- Oil or preservative content
- Evaporation residue
- Nitrite levels

Lubricant analyses and contamination identification

- Dissolution and filitration
- Microscopy
- FTIR analysis

Surface treatments

- Gold plating
- Ultrasonic cleaning
- Hot and cold black-oxide-finishing
- Passivation of high-alloy steels

Medical hygiene treatments

- High-pressure steam sterilisation
- Thermal disinfection

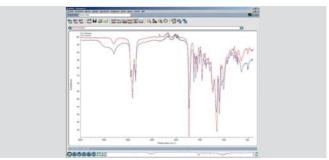
Condensation and salt spray test

Chemical deburring

For natural fiber reinforced polymers



benefit from flexible and cost-effective solutions developed in collaboration with their experienced GRW analyst's and chemistry lab team using state-of-the-art technical equipment.



FTIR spectra make the difference visible e.g.: A grease with water entrainment and a changed base oil-thickener-ratio compared to a fresh grease.

As part of our laboratory association, GRW offers you the following additional services:

SEM analysis (SEM) and energy-dispersive X-ray spectroscopy (EDX)

X-ray fluorescence analysis (RFA)

Detailed analysis by means of **Differential scanning calorimetry (DSC)**

Thermogravimetry (TGA)

Please contact us to learn more about the GRW laboratory services.





Correct handling of GRW high-precision miniature bearings

GRW ball bearings are manufactured and packaged with extreme care to avoid contamination, corrosion, and other external influences on the bearings. When mounting the ball bearings, the following advice is recommended:

- Bearings should be stored in their original package in clean, dry rooms under constant temperature conditions.
- Bearings should only be removed from their original package shortly before they are mounted. The use of gloves, finger cots, and tweezers are recommended.
- Care should be taken that the assembly location is clean and well lit and that all other parts are equally clean. A hard surface is preferred.
- When mounting a ball bearing, the assembly force must not be applied to the balls. Suitable mounting tools must be used. Non-compliance with these instructions may easily result in damage of balls or raceways, for example ball indentations may occur in the raceway.
- If glued interfaces are used, ensure that any excess glue does not enter the bearing.
- Re-lubrication should only be carried out with a lubricant of the same type and purity.

- We recommend to have the bearings lubricated by GRW, as this is executed in the clean room shortly before packaging.
- Selective sorting of all mating parts will help to guarantee the proper fit of the bearing to the shaft or housing.
- We recommend a run-in process for grease-lubricated bearings prior to use at low speed to achieve optimum distribution of the lubricant.
- Electrical current running through the bearing should be avoided

Analysis of ball bearings

Based on over 70 years of expertise, GRW can provide ball bearing analysis to establish the root cause of failure or to estimate the remaining life of the ball bearing. For more information about bearing analysis, please contact your nearest GRW Sales Representative.

Valuable results can be achieved when bearings are disassembled and examined after a certain period of operation before failure has occurred. Marking of the bearing rings during disassembly can help to reproduce original assembly characteristics.



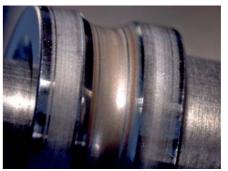


Installation on the shaft

Characteristics caused by improper handling

	Possible cause											
Defect characteristics	Contami- nation	Assembly	Assembly tools	Adhesive	Lubricant	Termpera- ture	Speed	Load	Storage	Ambient media	Fitting/ contact	Design
Increasin g running noise	X	х		Х	Х							Х
Mounting oble m s			х								Х	х
Bearing ockin g l	х	х		х		х	Х	х		х	х	
Corrosion	х								х	х	Х	
Coloration						х				Х		
Breakage								Х			Х	





Ball indentation in raceway

Ball bearing in dry running

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90 I





Indentations in raceway caused by particles



Packaging

Correct packaging protects bearings from contamination, corrosion and damage during transport and storage. We recommend that the package is opened just prior to mounting and that bearings from opened packages will be used as soon as possible. Each bearing package is labeled with the exact design specification and the respective product lot number, factory batch number, and the packaging date of the bearing.

Our Standard packaging options are as follows:

Strip Packaging "CP"

Our standard packaging contains ball bearings in one strip or pill pack, sealed individually in transparent synthetic film packets with a white backing. The quantity per strip depends on the outside diameter of the bearing.

Vacuum Packaging "LL"

Bearings are bulk packaged in a transparent synthetic film pack and sealed under vacuum. The quantity per vacuum pack depends on the size of the bearing or as specified by the customer.

Spindle bearing Packaging "CP1P"

Spindle bearings are sealed in a separate envelope marked "GRW" (CP1) and boxed individually (CP1P) to avoid damage.

Special Packaging

Packaging can be customised according to your specifications relative to the outside diameter of the respective bearing. GRW offers a wide range of packaging options, including placing the bearings on a metal stick, for automated assembly, and special aluminum envelopes.









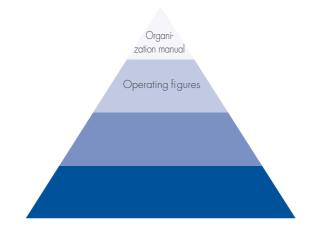
GRW quality: Internationally certified DIN EN ISO 9001

GRW is an international enterprise specialising in the development and production of high-precision miniature ball bearings. Ensuring our customers' complete satisfaction is our top priority. By continually improving our products and processes, we ensure the long- term success of our company.

To achieve these goals, we introduced a management system that evolves with the future requirements of each market. Our corporate strategy, based on growth and innovation, is the basis for a successful partnership with our customers and suppliers.

Our integrated management system is based on DIN EN ISO 9001:2008 and is certified in four specific areas:

- 1. Organisational Manual
- 2. Key Performance Indicators (KPI)
- 3. Process Definitions and defined Responsibilities
- 4. Process Control Documentation (work and test instructions) including supporting documents (e.g. quality check lists, forms)



The Organisational Manual includes a Management section addressing our customers, employees and suppliers. It contains our corporate principles and corporate policy. Special sections contain job descriptions and Key Performance Indicators. These critical areas of measurement contain the controlling documentation for organisational process and product quality as well as continuous improvement.







Manufacturing in a nut shell

GRW high-precision ball bearings are used in a variety of industries and applications. Before they leave our factory they have passed several complex, manufacturing steps.

Their journey starts in the turning department where our high-precision turning machines produce bearing rings from a variety of steels used by GRW.



Turning department



since 1947



www.grw.de

Honing is the last step before assembly. The finished, bearing rings run through a final process on machines co-developed by GRW for surface finishing of the raceways.

During the final assembly, finished components are sorted and selected to guarantee customer satisfaction and in some cases automated assembly can be used to assemble, lubricate and package bearings.

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After heat treatment, all critical dimensions and raceway geometries are precisely machined and ground to the micron (µ). Interim quality inspection is carried out in the measurement room.





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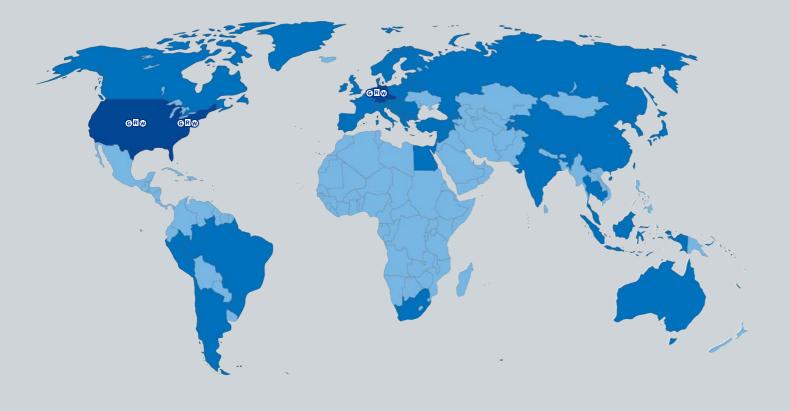
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As of: 11/13







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